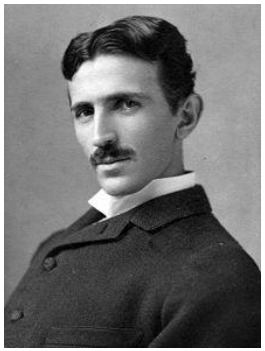
ELEKTROMOTORNI POGONI SA ASINHRONIM MOTOROM

Proučavamo samo pogone sa trofaznim motorom.

Najčešće korišćeni motor u elektromotornim pogonima.

Prednosti asinhronih motora:

- jednostavna konstrukcija;
- mala cena;
- visoka energetska efikasnost.

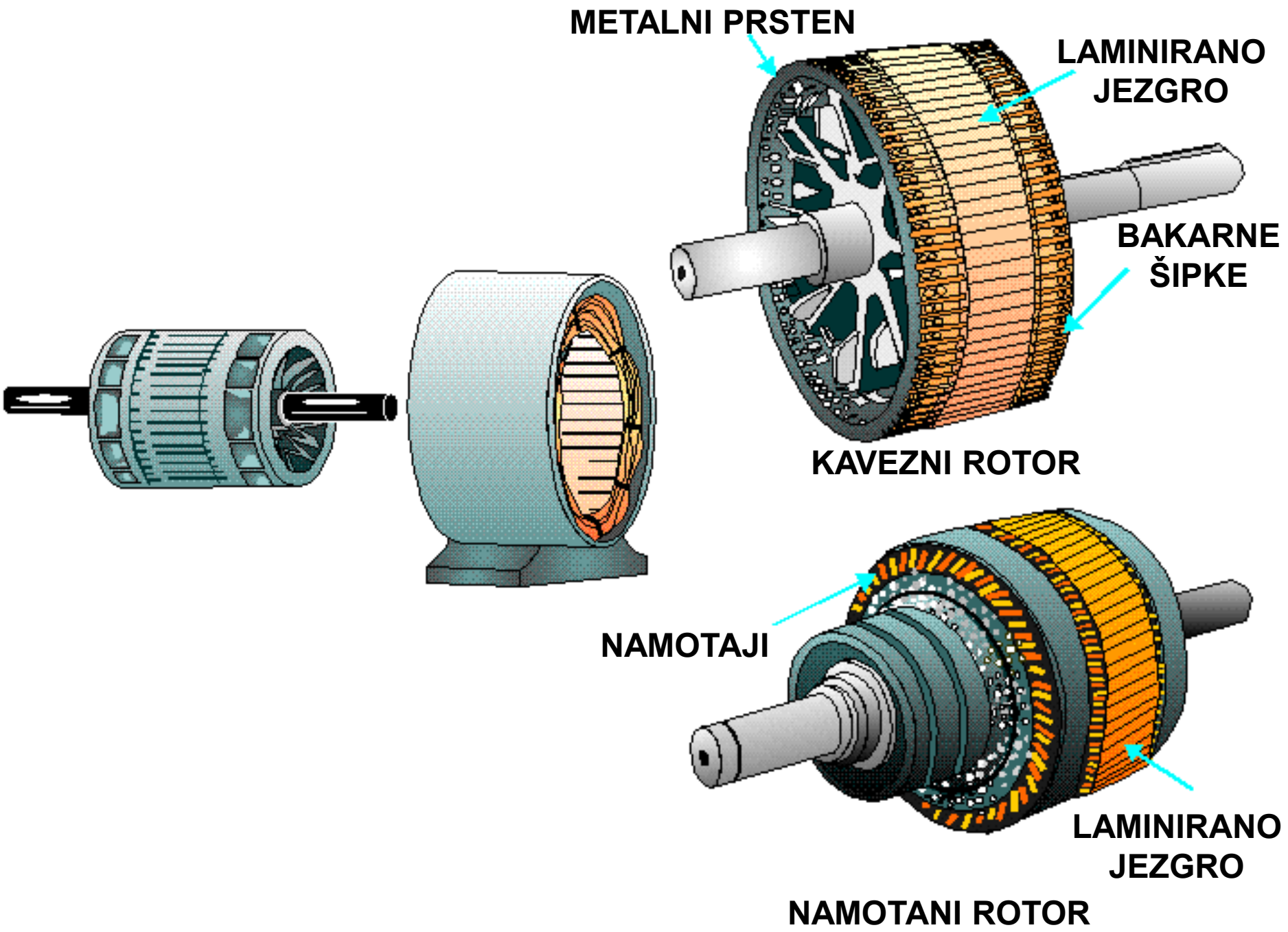


Nikola Tesla

1856-1943

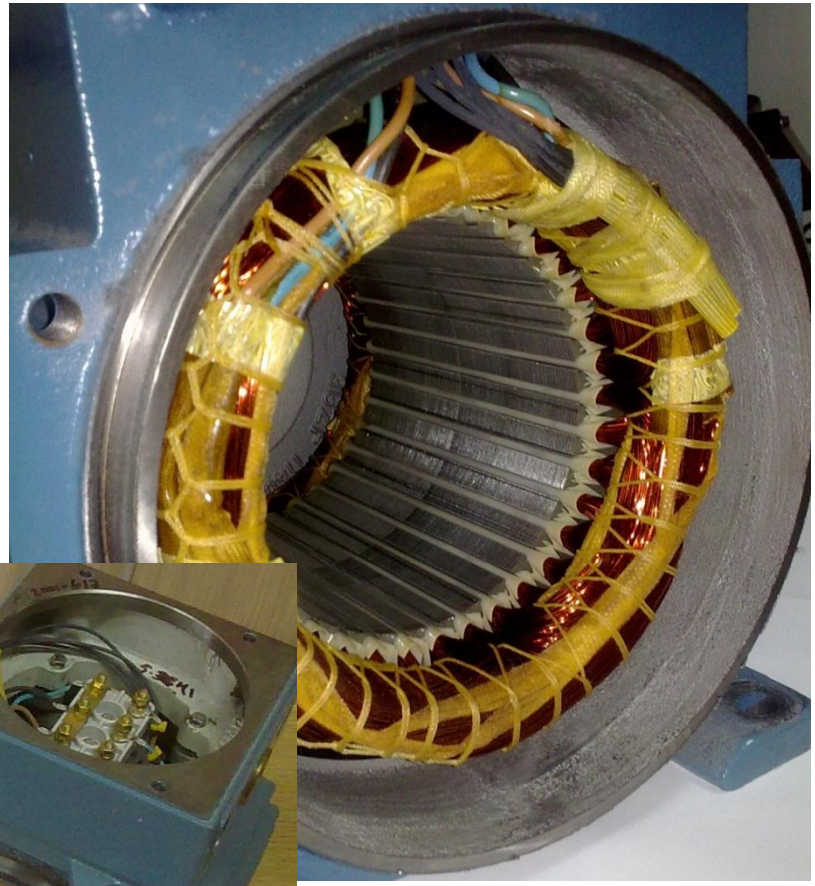


Asinhroni (indukcioni) motor
Patent iz 1888 godine


METALNI PRSTEN
LAMINIRANO JEZGRO
BAKARNE ŠIPKE
KAVEZNI ROTOR
NAMOTAJI
LAMINIRANO JEZGRO
NAMOTANI ROTOR

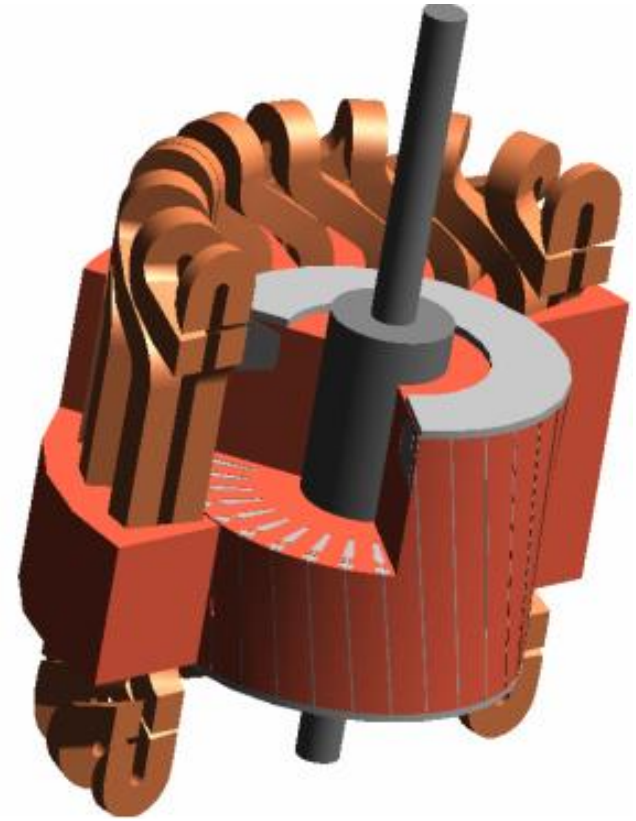
Motor sa kaveznim rotorom

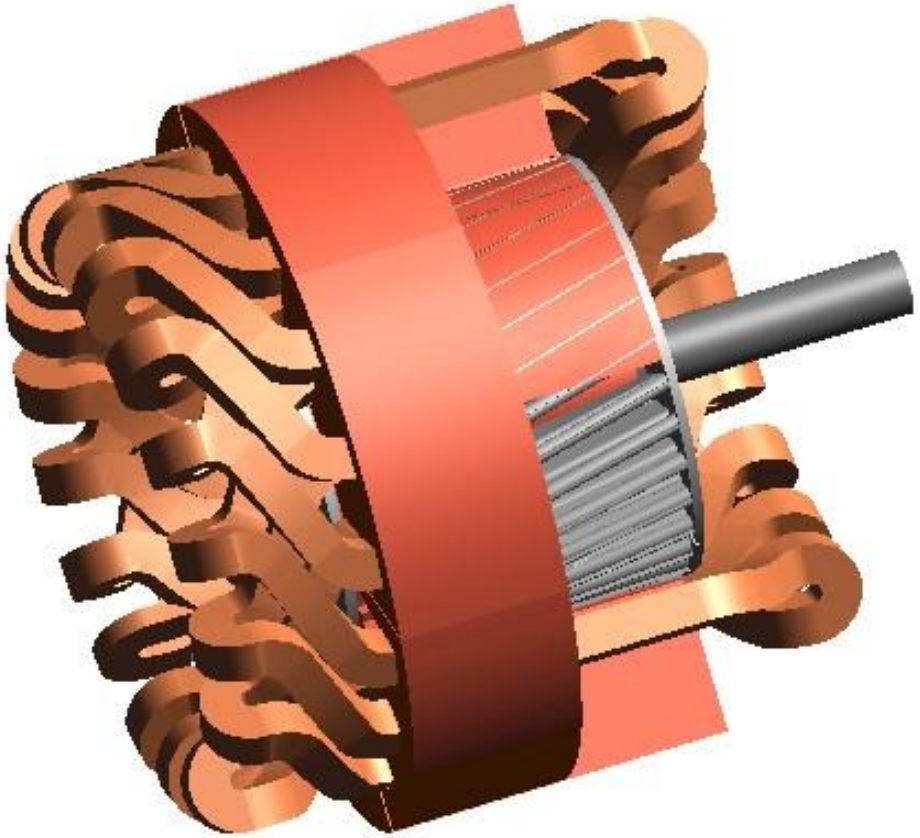
Stator



Rotor







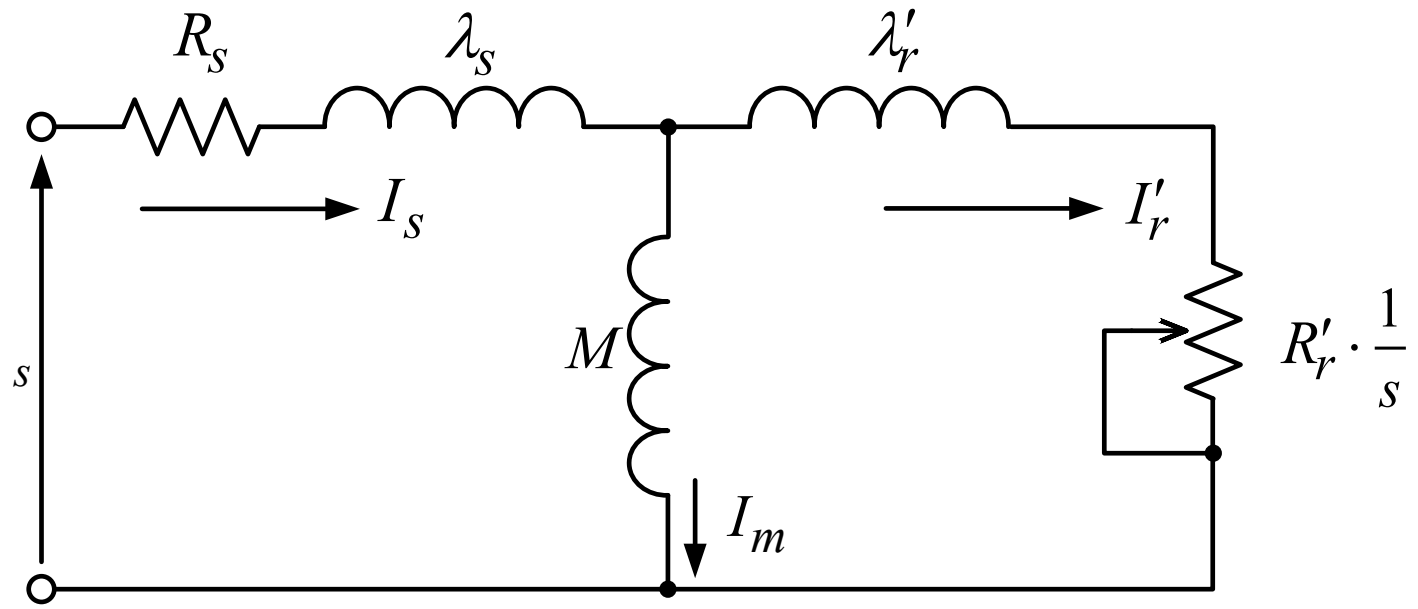
ROTOR ASINHRONOG MOTORA NAJČEŠĆE IMA ZAKOŠENE ŽLEBOVE DA BI SE MINIMIZIRALE PULSACIJE MOMENTA

POPREČNI PRESEK ASINHRONOG MOTORA



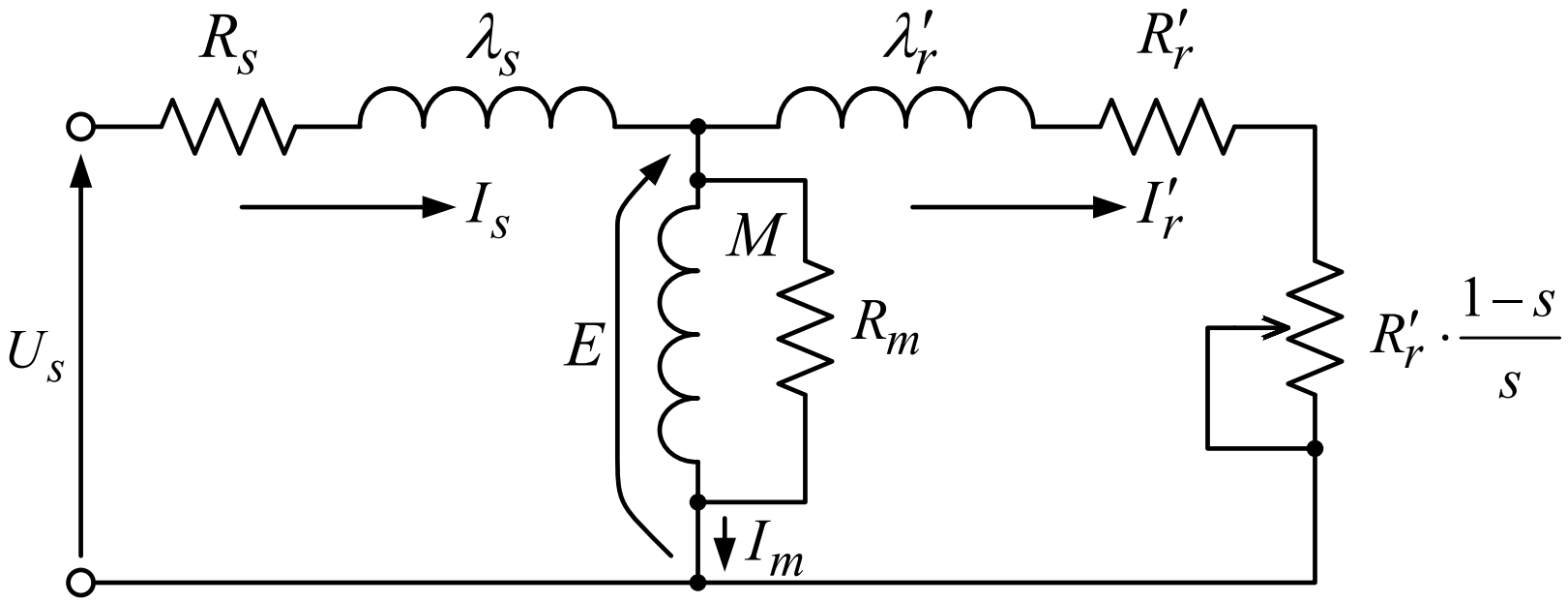
STATIKA POGONA

Ekvivalentna šema motora (po fazi).



Rotorske veličine su svedene na stator.

Ekvivalentna šema motora (po fazi) sa razdvojenim gubicima u bakru rotora.



Rotorske veličine su svedene na stator.

Ostale karakteristične veličine:

$f_s \left[\mathrm{Hz}\right]$ - statorska učestanost;

$f_r \left[\mathrm{Hz}\right]$ - rotorska učestanost;

$\omega_s = 2\pi \cdot f_s \left[\mathrm{rad.el./s}\right]$ - kružna učestanost statora ili električna sinhrona brzina ili brzina obrtnog polja (električna)

$\omega_r = 2\pi \cdot f_r \left[\mathrm{rad.el./s}\right]$ -kružna učestanost rotora;
U knjizi: apsolutno klizanje

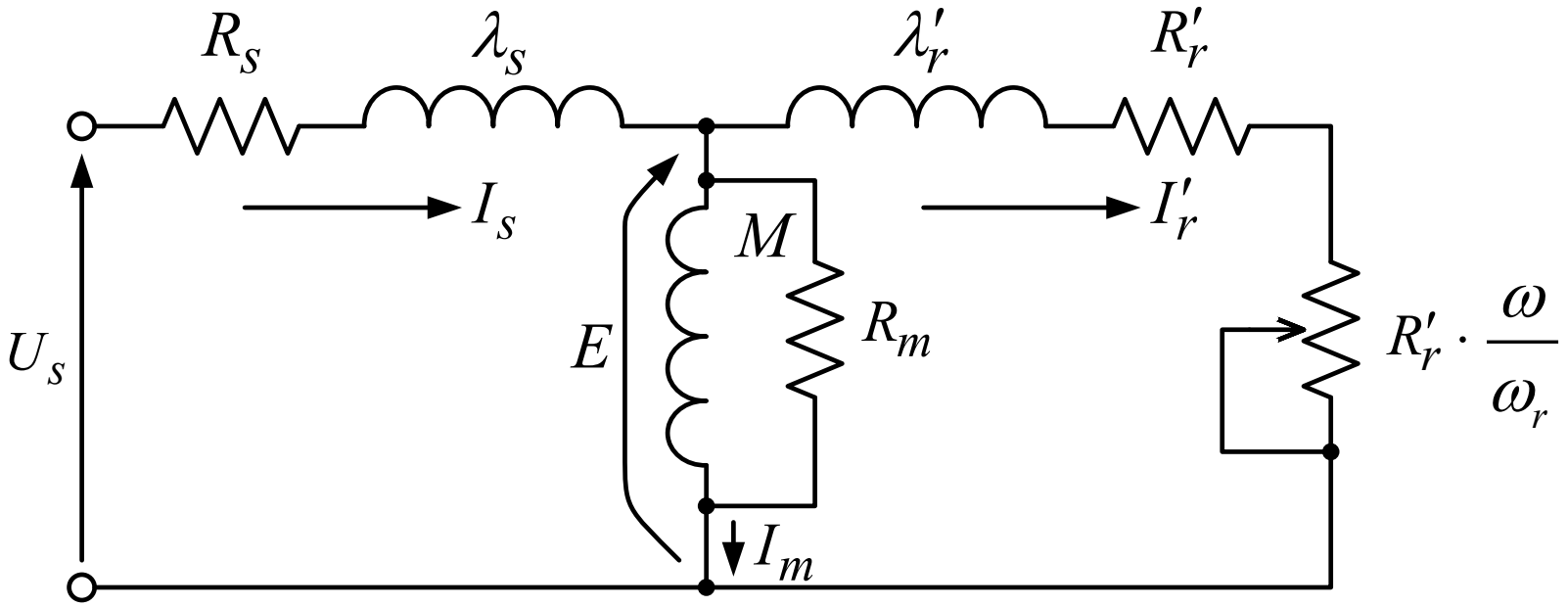
$\omega = \omega_s - \omega_r \left[\mathrm{rad.el./s}\right]$ - ugaona brzina (**električna**);

P - broj pari polova;

$\omega_m = \omega / P \left[\mathrm{rad.meh./s = rad/s}\right]$ - mehanička ugaona brzina;

$s = \omega_r / \omega_s = \left(\omega_s - \omega\right) / \omega_s$ - klizanje.

Ekvivalentna šema motora (po fazi), razdvojeni gubici u bakru rotora, ne koristi se **klizanje**.



Rotorske veličine su svedene na stator.

$$\frac{1-s}{s} = \frac{\omega_s - \omega_r}{\omega_r}$$

Klizanje je veličina pogodna za analizu rada asinhronih mašina sa konstantnom učestanošću napajanja statora (iz mreže).

Može se koristiti i pri promenljivoj učestanosti statora, ali uz uvažavanje:

$$s = \frac{\omega_r}{\omega_s}$$

BAZNE VREDNOSTI

$U_b = U_{sn}$ – nominalna efektivna vrednost faznog napona

$I_b = I_{sn}$ – nominalna efektivna vrednost fazne struje

$\omega_b = 2\pi f_{sn}$ – nominalna kružna učestanost (električna)

Bazna impedansa: $Z_b = U_b / I_b$

Bazna snaga: $P_b = q\ U_b\ I_b = 3\ U_b\ I_b$ q - broj faza = 3

Bazni moment: $M_b = P_b / (\omega_b / P)$

TOKOVI SNAGE

$P_s = 3 \cdot U_s \cdot I_s \cdot \cos\varphi_s$ - snaga statora, snaga uzeta iz izvora;

$P_{s\,Cu} = 3 \cdot R_s \cdot I_s^2$ - snaga gubitaka u bakru statora;

$P_{Fe} = 3 \cdot E^2 / R_m$ - snaga gubitaka u gvožđu $\left(\lim_{R_m \to \infty} P_{Fe} \to 0 \right)$

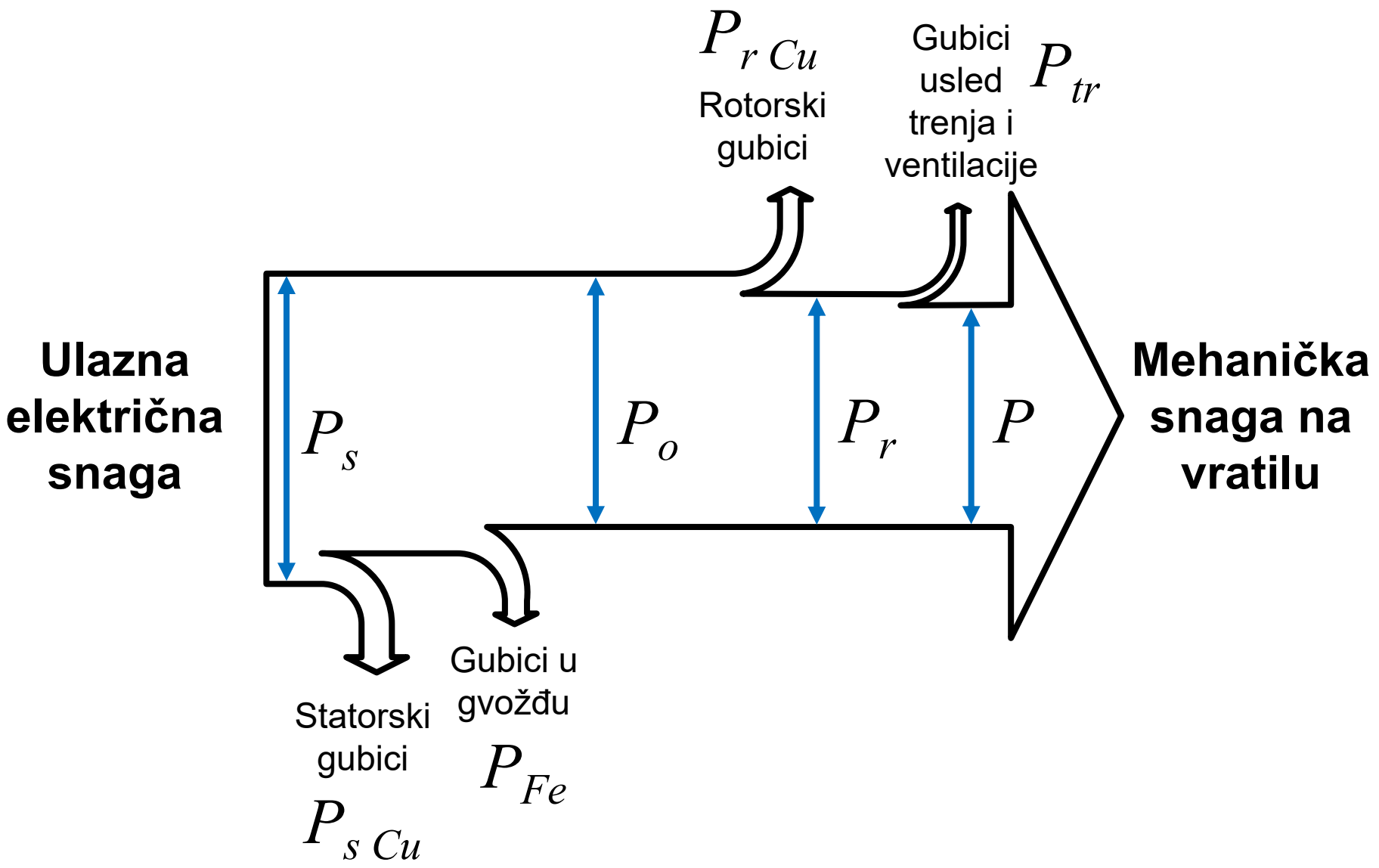
$P_o = 3 \cdot \left(R'_r / s \right) \cdot \left(I'_r \right)^2$ - snaga obrtnog magnetnog polja;

$P_{r\,Cu} = 3 \cdot R'_r \cdot \left(I'_r \right)^2 = s \cdot P_o$ - snaga gubitaka u bakru rotora;

$P_r = P_o - P_{r\,Cu} = 3 \cdot R'_r \cdot \frac{1-s}{s} \cdot \left(I'_r \right)^2 = \left(1 - s \right) \cdot P_o$ - mehanička snaga;

P_{tr} - snaga gubitaka na trenje i ventilaciju;

$P = P_r - P_{tr}$ - korisna mehanička snaga.



<u>Napomena</u>: Snaga P_{tr} prenosi se u opterećenje!

Elektromagnetni moment:

$$M_e = \frac{P_r}{\omega_m} = \underbrace{3 \cdot R'_r \cdot \frac{1-s}{s} \cdot \left(I'_r\right)^2}_{P_r} \cdot \frac{1}{\omega_m} =$$

$$= 3 \cdot R'_r \frac{1-s}{s} \cdot \left(I'_r\right)^2 \cdot \left(\frac{\omega_s}{\omega_s}\right) \cdot \frac{P}{\omega} =$$

$$= 3 \cdot P \cdot \frac{R'_r}{s} \cdot \frac{\left(I'_r\right)^2}{\omega_s} = 3 \cdot P \cdot R'_r \frac{\left(I'_r\right)^2}{\omega_r}$$

MEHANIČKA KARAKTERISTIKA
(statička karakteristika momenta)

U PREDSTOJEĆOJ ANALIZI PRETPOSTAVIMO DA JE E = const.

$$M_e = M_e(\omega)$$

$$\left|I'_r(s)\right| = \frac{\left|E\right|}{\sqrt{\left(R'_r/s\right)^2 + \left(\omega_s \cdot \lambda'_r\right)^2}}$$

$$M_e(s) = 3 \cdot P \cdot \frac{E^2}{\omega_s} \frac{R'_r/s}{\left(R'_r/s\right)^2 + \left(\omega_s \cdot \lambda'_r\right)^2}$$

$$M_e(\omega_r) = 3 \cdot P \cdot \left(\frac{E}{\omega_s}\right)^2 \frac{\omega_r \cdot R'_r}{\left(R'_r\right)^2 + \left(\omega_r \cdot \lambda'_r\right)^2}$$

Funkcija $M_e(s)$ ima ekstremum koji se može naći iz:

$$\frac{dM_e(s)}{ds} = 0$$

Momenat u tački ekstremuma naziva se *PREVALNI MOMENT* (M_p),
a odgovarajuće klizanje *PREVALNO KLIZANJE* (s_p).

$$s_p = \pm \frac{R'_r}{\omega_s \cdot \lambda'_r}; \qquad M_p = \pm \frac{3 \cdot P}{2} \cdot \left(\frac{E}{\omega_s} \right)^2 \frac{1}{\lambda'_r}$$

***KLOSS* - ova FORMULA**

$$\frac{M_e}{M_p} = \frac{2}{\frac{s}{s_p} + \frac{s_p}{s}} = \frac{2}{\frac{\omega_r}{\omega_{rp}} + \frac{\omega_{rp}}{\omega_r}}$$

Važno:

$$\omega_{rp} = \omega_s \cdot s_p = \pm \frac{R'_r}{\lambda'_r} = \text{const.}$$

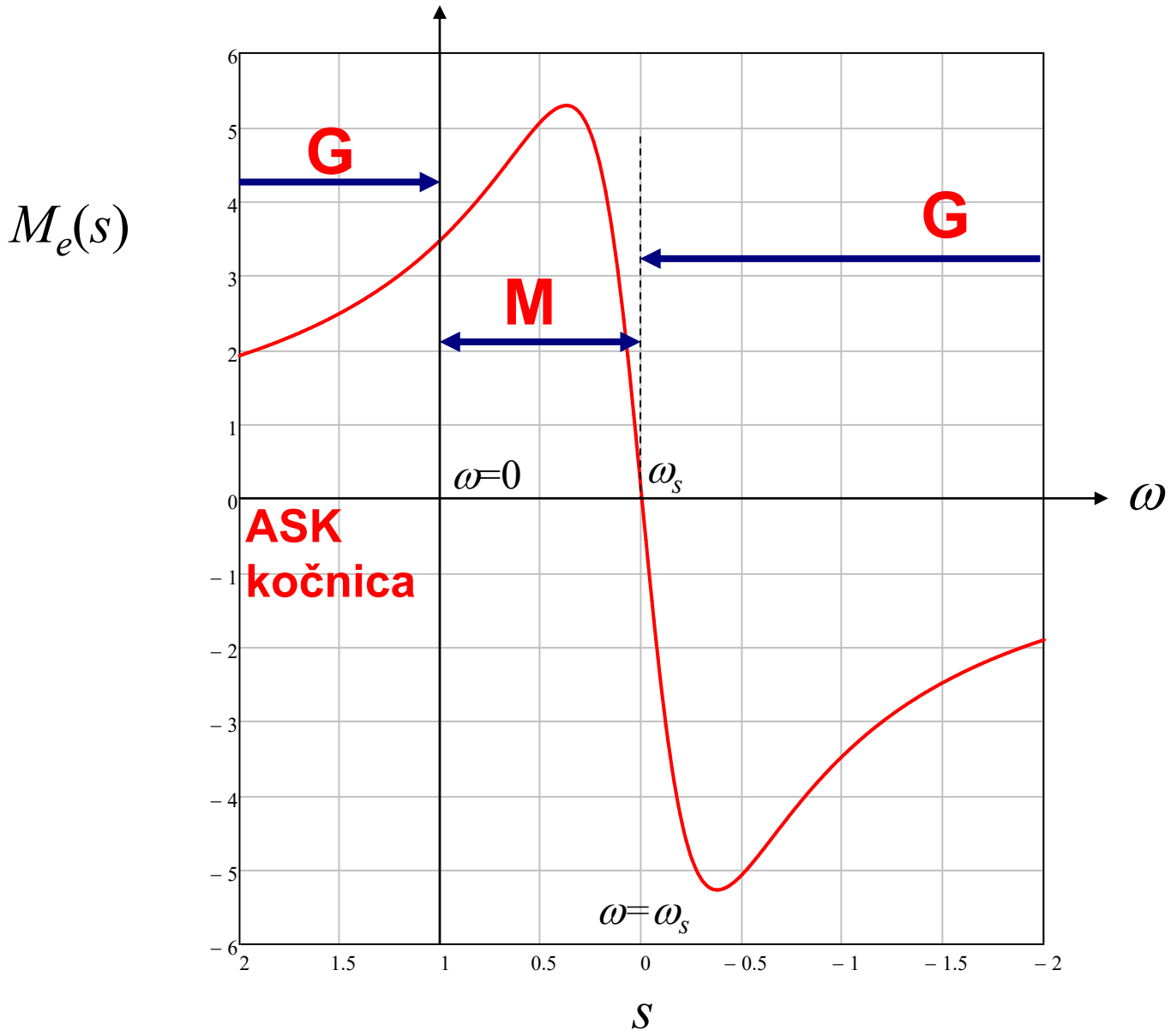
STATIČKE KARAKTERISTIKE STRUJA

$$\vec{I}_s = \vec{I}'_r + \vec{I}_m$$

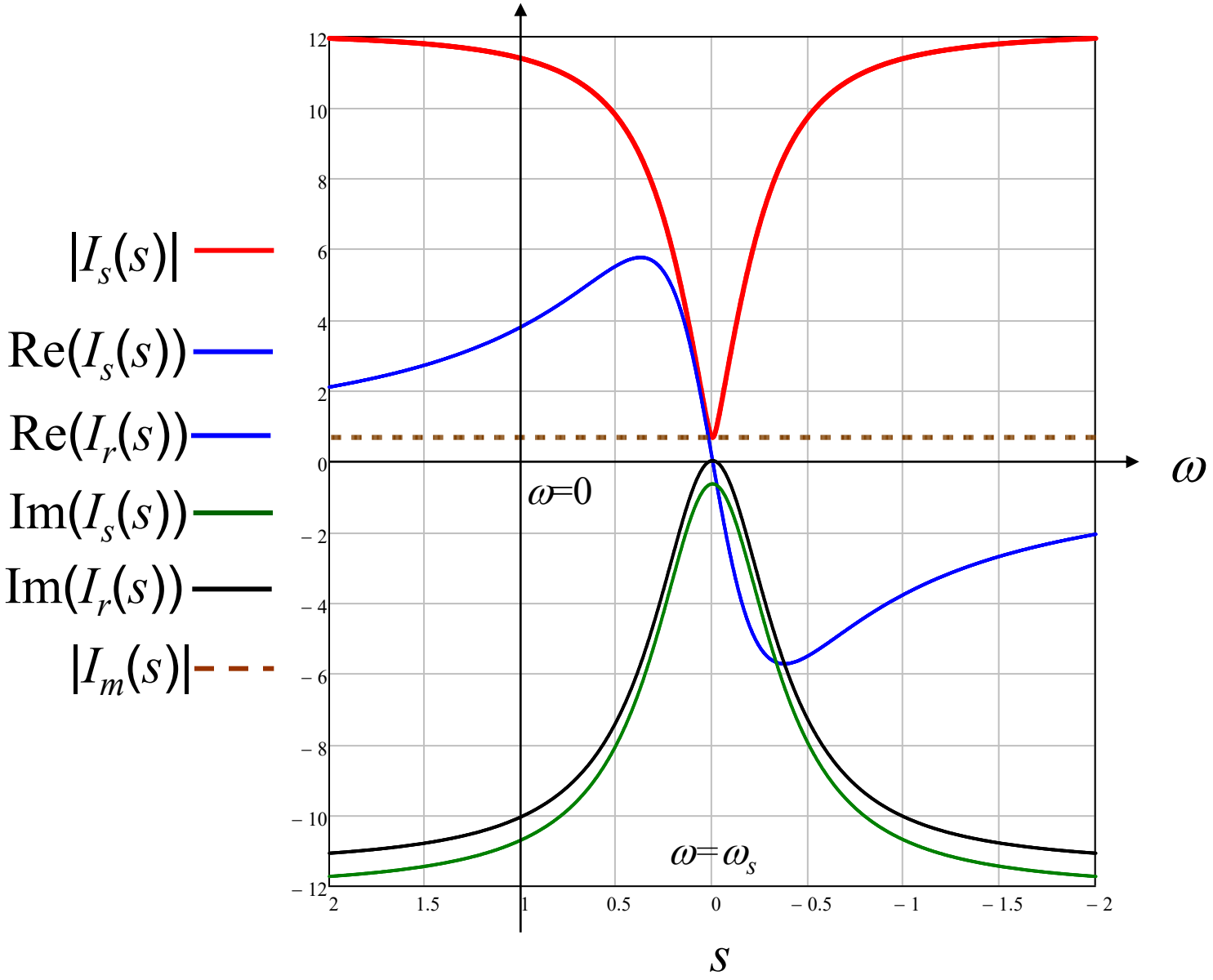
$$\vec{I}'_r = \frac{E \cdot R'_r / s}{\left(R'_r / s\right)^2 + \left(\omega_s \cdot \lambda'_r\right)^2} - j \frac{E \cdot \omega_s \cdot \lambda'_r}{\left(R'_r / s\right)^2 + \left(\omega_s \cdot \lambda'_r\right)^2} = I'_{ra} - jI'_{rr}$$

$$\vec{I}_m = -j \frac{E}{\omega_s \cdot M} \qquad \text{za} \quad P_{Fe} \approx 0 \quad \text{ili} \quad \left(R_m \to \infty\right)$$

Statička karakteristika momenta, pri E=const.



Statičke karakteristike struja, E=const.



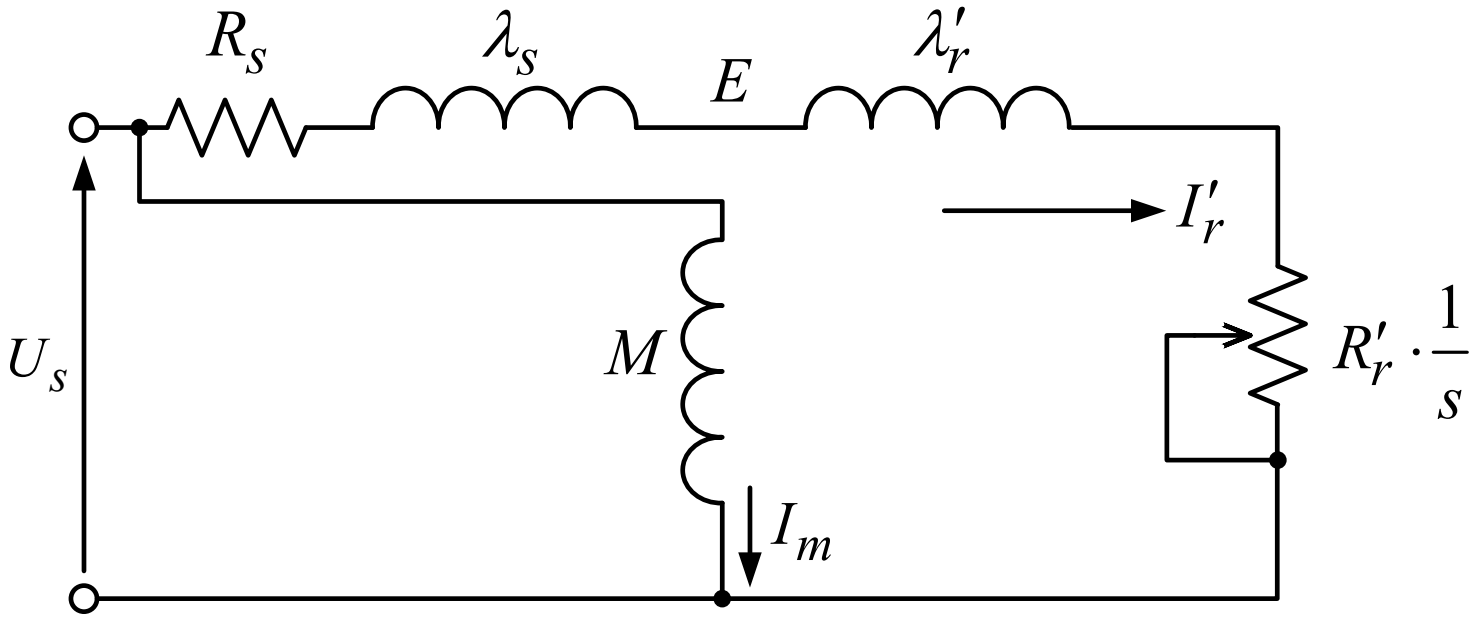
RAZMOTRIMO REALAN (realniji) SLUČAJ

$$E \neq \text{const.} \quad U_s = \text{const.}$$

Dve pretpostavke:

1. $P_{Fe} = 0 \quad \Rightarrow \quad R_m \to \infty$

2. $\omega_s^2 \cdot M^2 >> R_s^2 + \omega_s^2 \cdot \lambda_s^2$ (sasvim realna pretpostavka)



Sa navedenim pretpostavkama se može napisati:

$$\left|\vec{I}'_r\right| = \frac{U_s}{\sqrt{\left(R_s + R'_r/s\right)^2 + \omega_s^2 \cdot \left(\lambda_s + \lambda'_r\right)^2}}$$

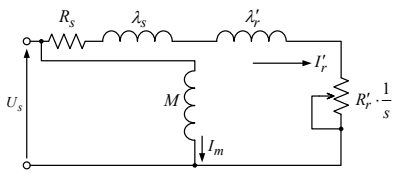
$$M_e = \frac{3 \cdot P \cdot U_s^2}{\omega_s} \frac{R'_r/s}{\left(R_s + R'_r/s\right)^2 + \omega_s^2 \cdot \left(\lambda_s + \lambda'_r\right)^2}$$

$$s_p = \pm \frac{R'_r}{\sqrt{R_s^2 + \omega_s^2 \cdot \left(\lambda_s + \lambda'_r\right)^2}} = f\left(\omega_s\right)$$

$$M_p = \pm \frac{3 \cdot P \cdot U_s^2}{2 \cdot \omega_s} \cdot \frac{1}{\sqrt{R_s^2 + \omega_s^2 \cdot \left(\lambda_s + \lambda'_r\right)^2} \pm R_s}$$

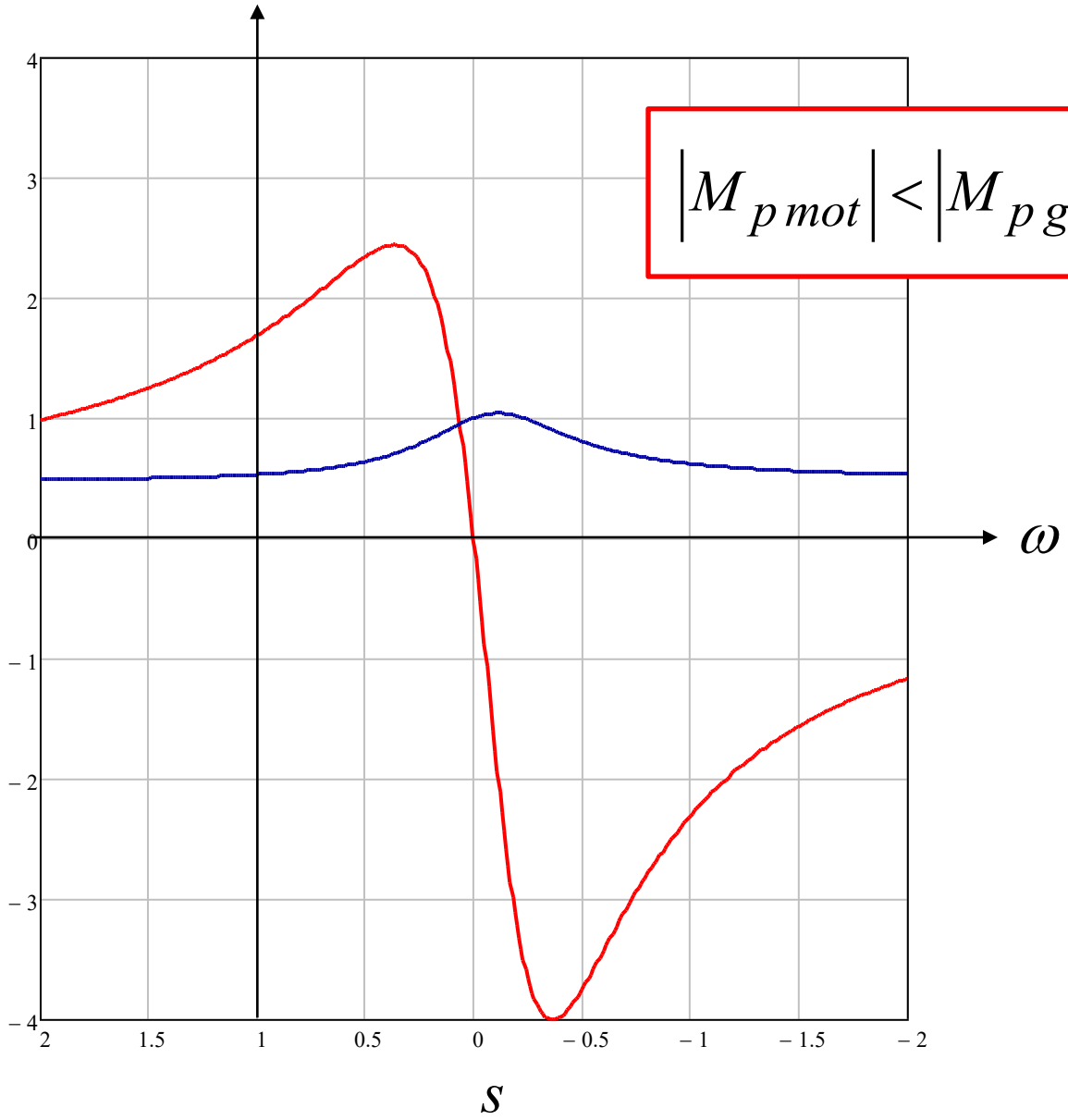
znaci: + za motorni režim;
− za generatorski režim.

Statička karakteristika momenta, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$



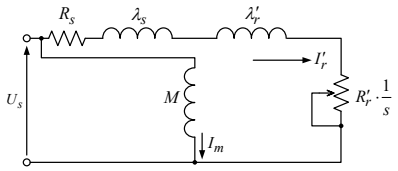
$M_e(s)$ —

$|E(s)|$ —



$$\left|M_{p\,mot}\right| < \left|M_{p\,gen}\right|$$

Statičke karakteristike struja, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$



$|I_s(s)|$

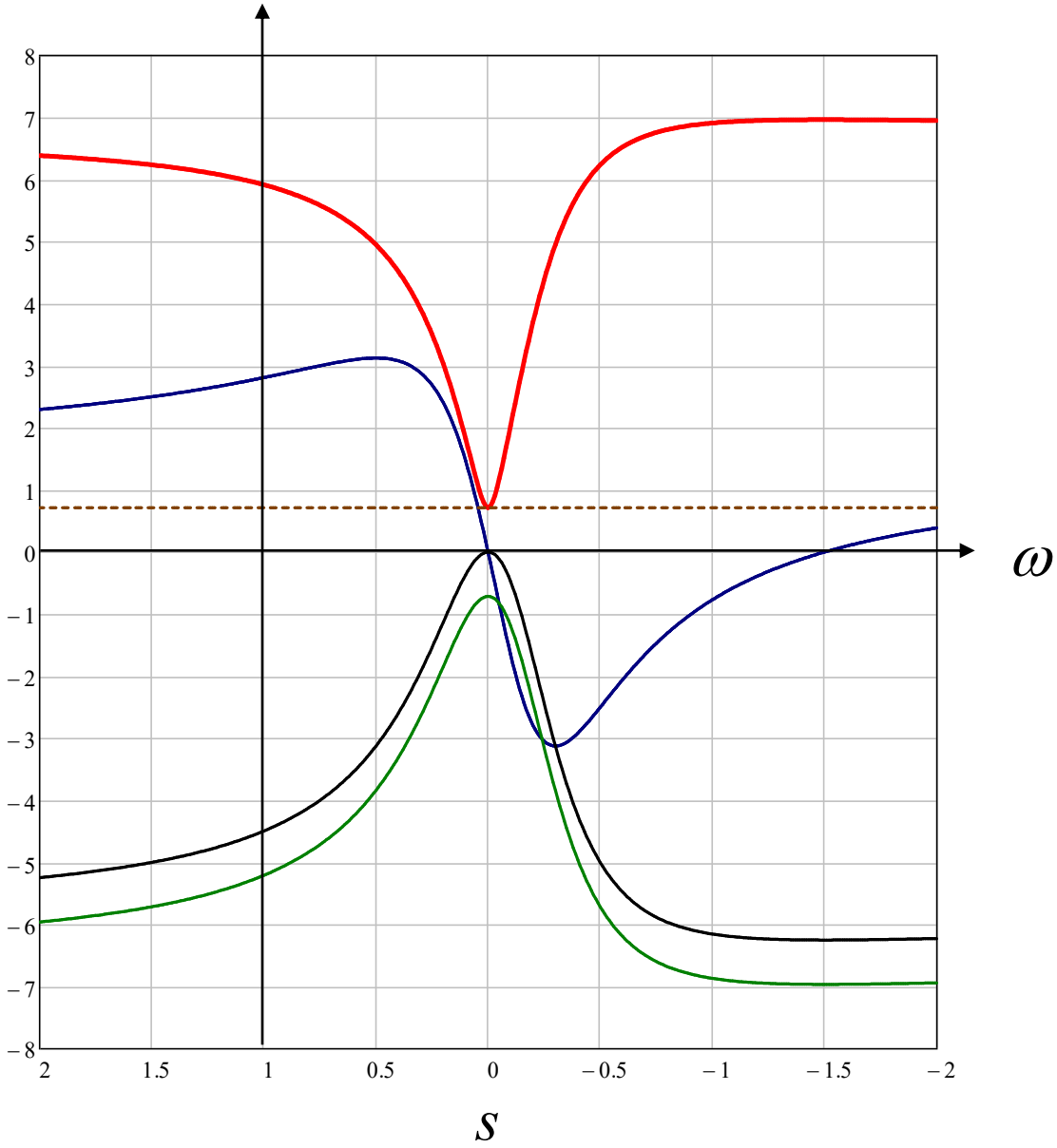
$\mathrm{Re}(I_s(s))$

$\mathrm{Re}(I_r(s))$

$\mathrm{Im}(I_s(s))$

$\mathrm{Im}(I_r(s))$

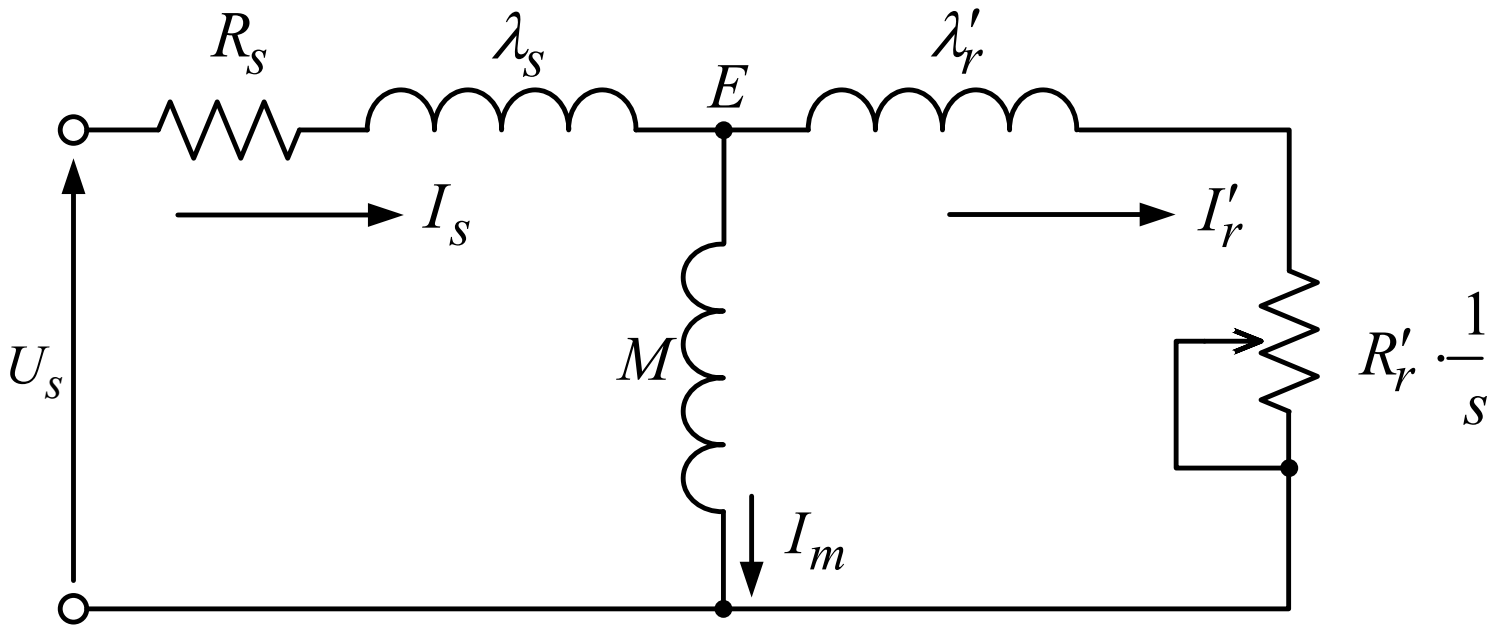
$|I_m(s)|$



RAZMOTRIMO SLUČAJ BEZ ZANEMARENJA INDUKTIVNOSTI MAGNEĆENJA

$$E \neq \text{const.} \quad U_s = \text{const.}$$

Jedina pretpostavka: $P_{Fe} = 0 \quad \Rightarrow \quad R_m \to \infty$



$$Z_s = R_s + j \cdot \omega_s \cdot \lambda_s \qquad Z'_r(s) = R'_r / s + j \cdot \omega_s \cdot \lambda'_r$$

$$Z_m = j \cdot \omega_s \cdot M$$

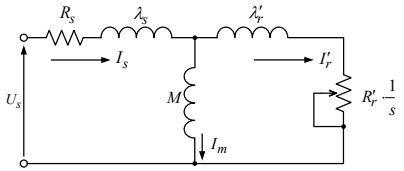
$$Z_e(s) = Z_s + Z_m \,||\, Z'_r(s)$$

$$\vec{U}_s = U_s + j \cdot 0 = U_s \qquad \vec{I}_s(s) = \frac{U_s}{Z_e(s)} \qquad \vec{E}(s) = U_s - Z_s \cdot \vec{I}_s$$

$$\vec{I}_m(s) = \frac{\vec{E}(s)}{Z_m} \qquad \vec{I}'_r(s) = \frac{\vec{E}(s)}{Z'_r(s)} = \vec{I}_s(s) - \vec{I}_m(s)$$

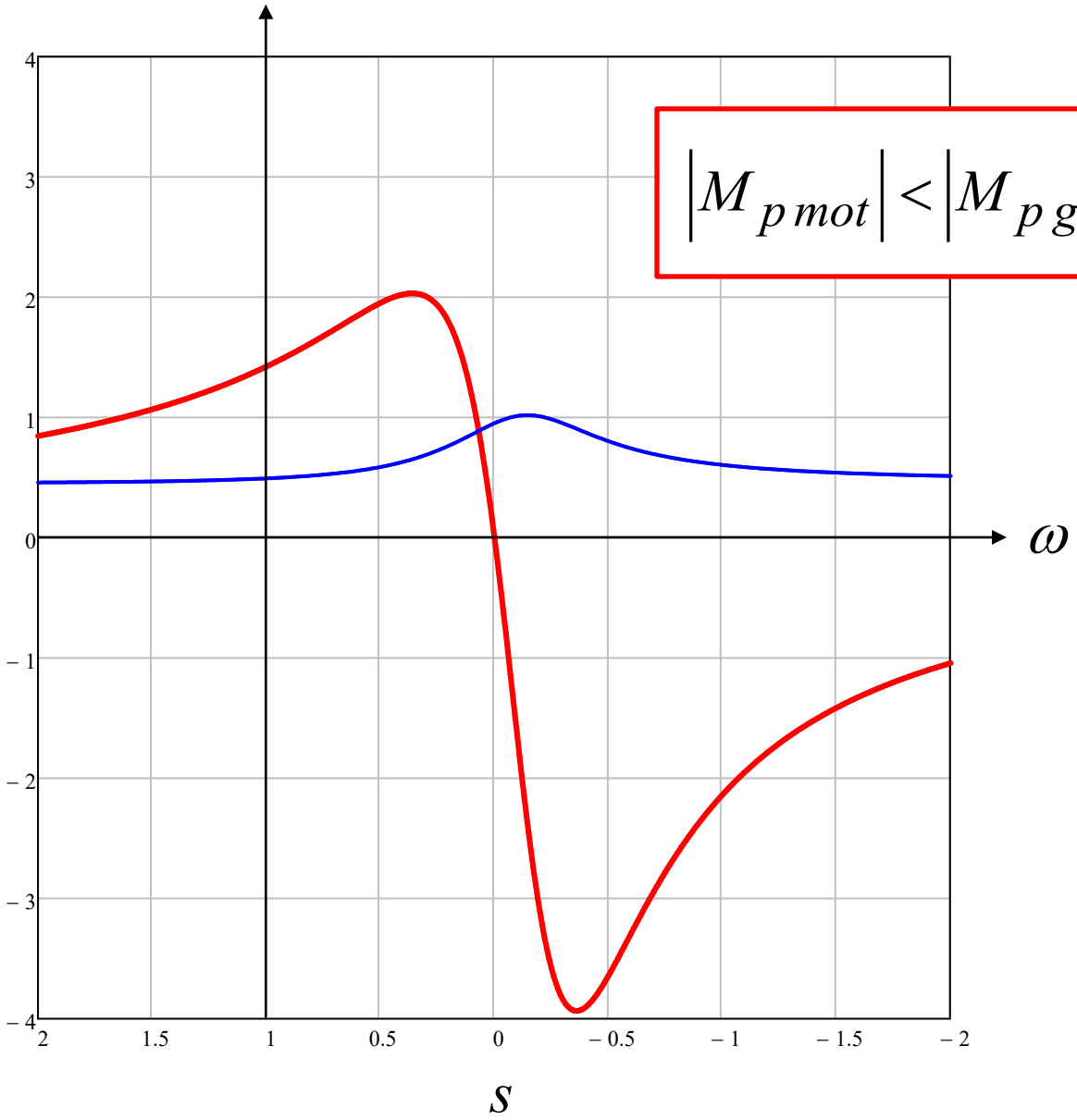
$$M_e = \frac{P_r}{\omega_m} = 3 \cdot P \cdot \frac{R'_r}{s} \cdot \frac{\left|\vec{I}'_r\right|^2}{\omega_s} = 3 \cdot P \cdot R'_r \frac{\left|\vec{I}'_r\right|^2}{\omega_r}$$

Statička karakteristika momenta, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$



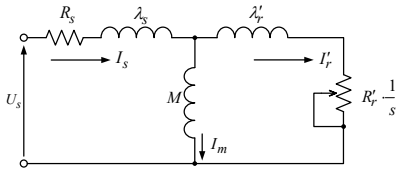
$M_e(s)$

$|E(s)|$



$$\left|M_{p\,mot}\right| < \left|M_{p\,gen}\right|$$

Statičke karakteristike struja, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$



$|I_s(s)|$

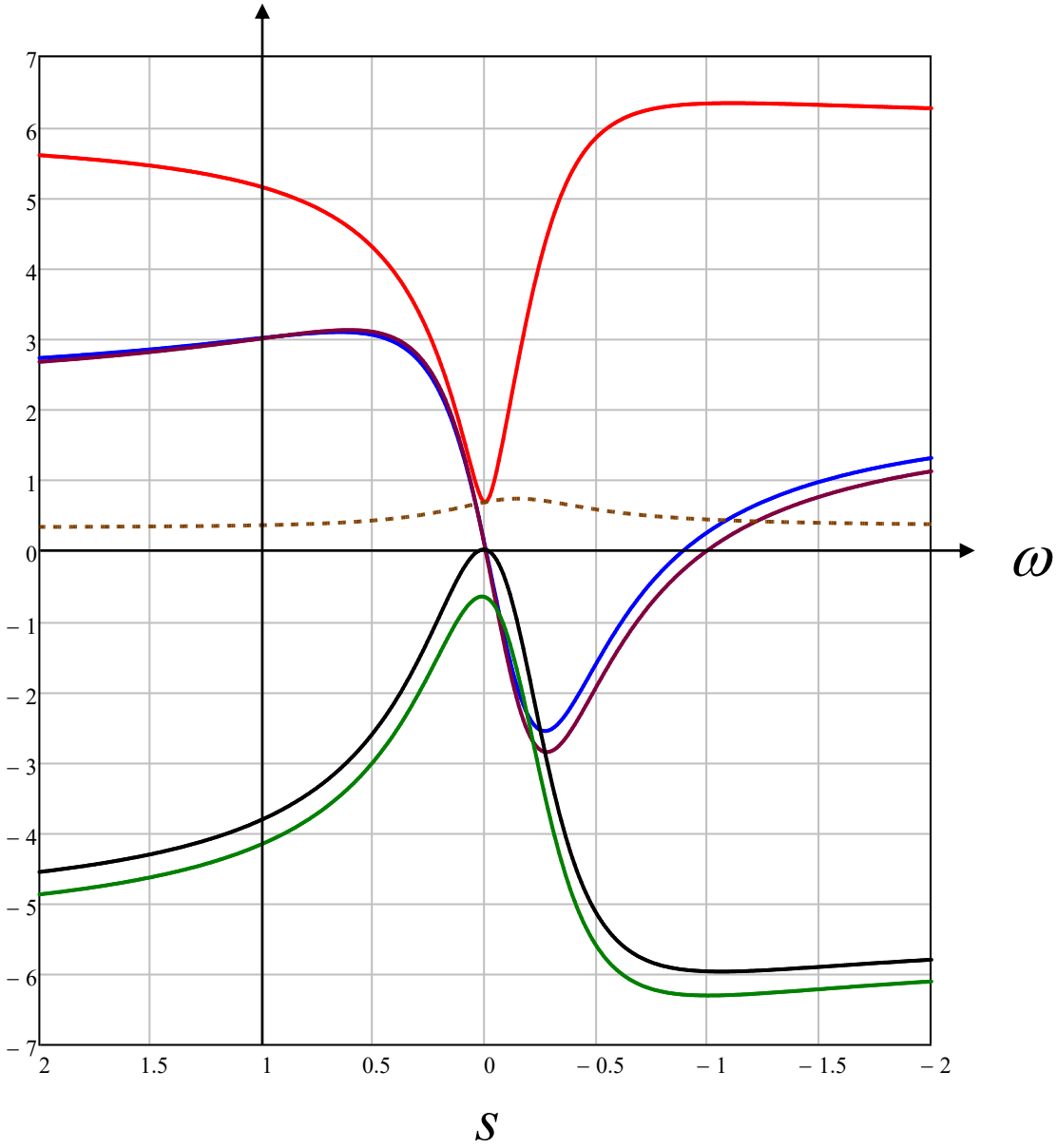
$\mathrm{Re}(I_s(s))$

$\mathrm{Re}(I_r(s))$

$\mathrm{Im}(I_s(s))$

$\mathrm{Im}(I_r(s))$

$|I_m(s)|$



Kod velikih mašina može se smatrati: $R_s \approx 0 \quad M \gg (\lambda_s, \lambda'_r)$

Sada je:

$$M_e \approx \frac{3 \cdot P \cdot U_s^2}{\omega_s} \cdot \frac{R'_r / s}{(R'_r / s)^2 + \omega_s^2 \cdot (\lambda_s + \lambda'_r)^2}$$

Analitički izraz momenta za Γ šemu

$$s_p = \pm \frac{R'_r}{\omega_s \cdot (\lambda_s + \lambda'_r)} \qquad \omega_s \cdot s_p = \omega_{rp} = \pm \frac{R'_r}{(\lambda_s + \lambda'_r)}$$

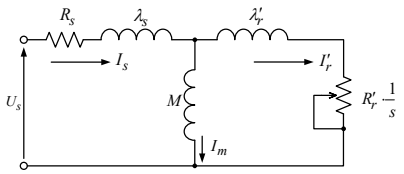
$$M_p = \pm \frac{3 \cdot P}{2} \cdot \left(\frac{U_s}{\omega_s} \right)^2 \cdot \frac{1}{\lambda_s + \lambda'_r}$$

Veoma slično kao kod *E*=const. Može se izvesti *KLOSS* - ova formula.

$$\frac{M_e}{M_p} = \frac{2}{\frac{s}{s_p} + \frac{s_p}{s}} = \frac{2}{\frac{\omega_r}{\omega_{rp}} + \frac{\omega_{rp}}{\omega_r}}$$

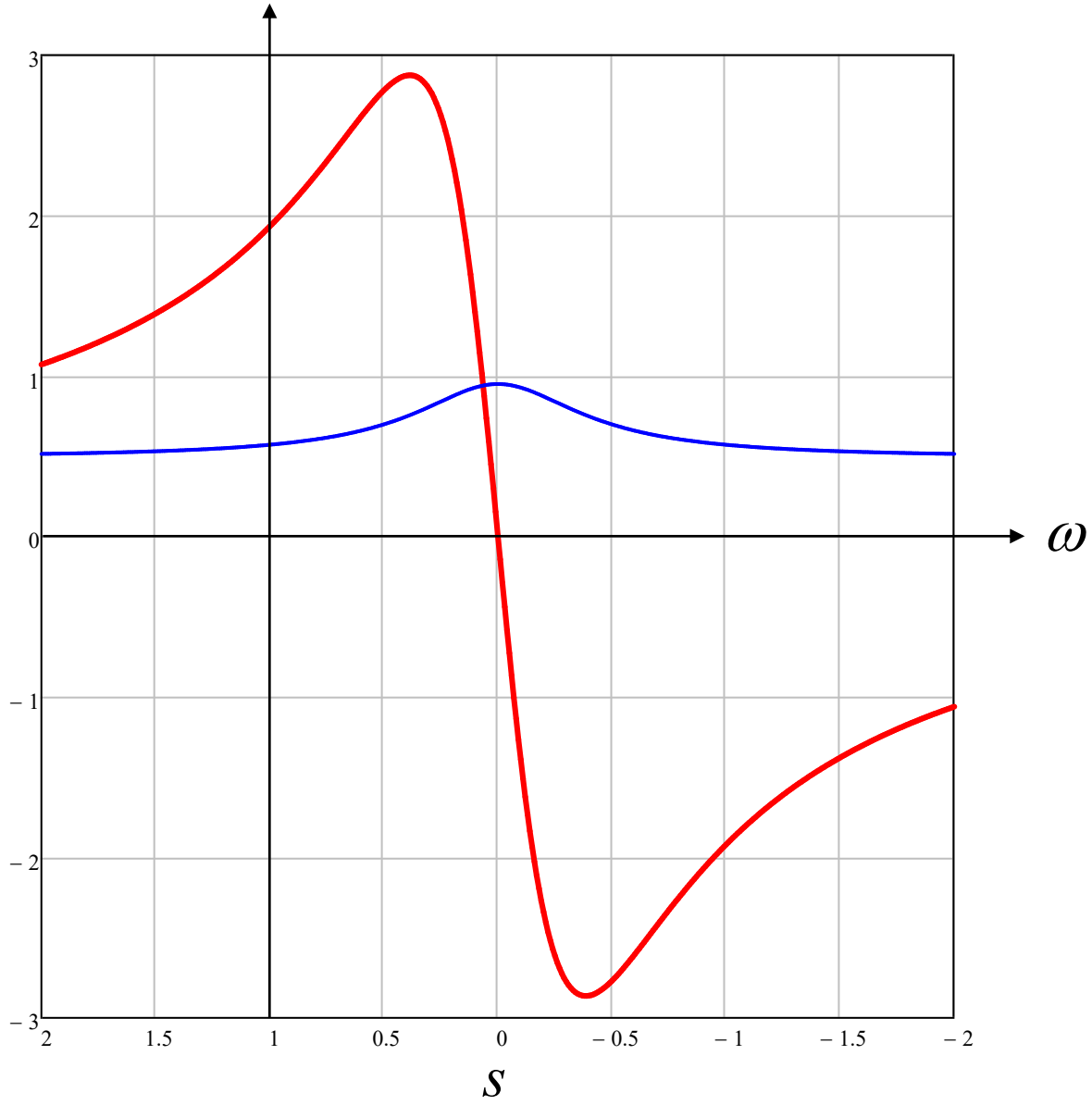
Statička karakteristika momenta, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$

$R_s = 0$



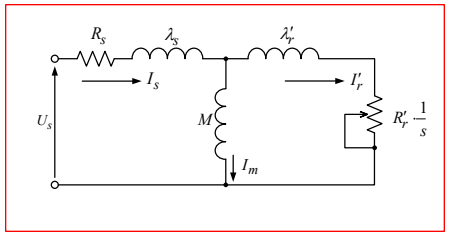
$M_e(s)$

$|E(s)|$



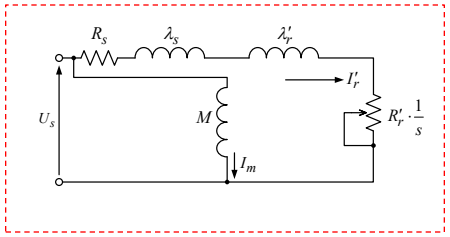
Statička karakteristika momenta, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$

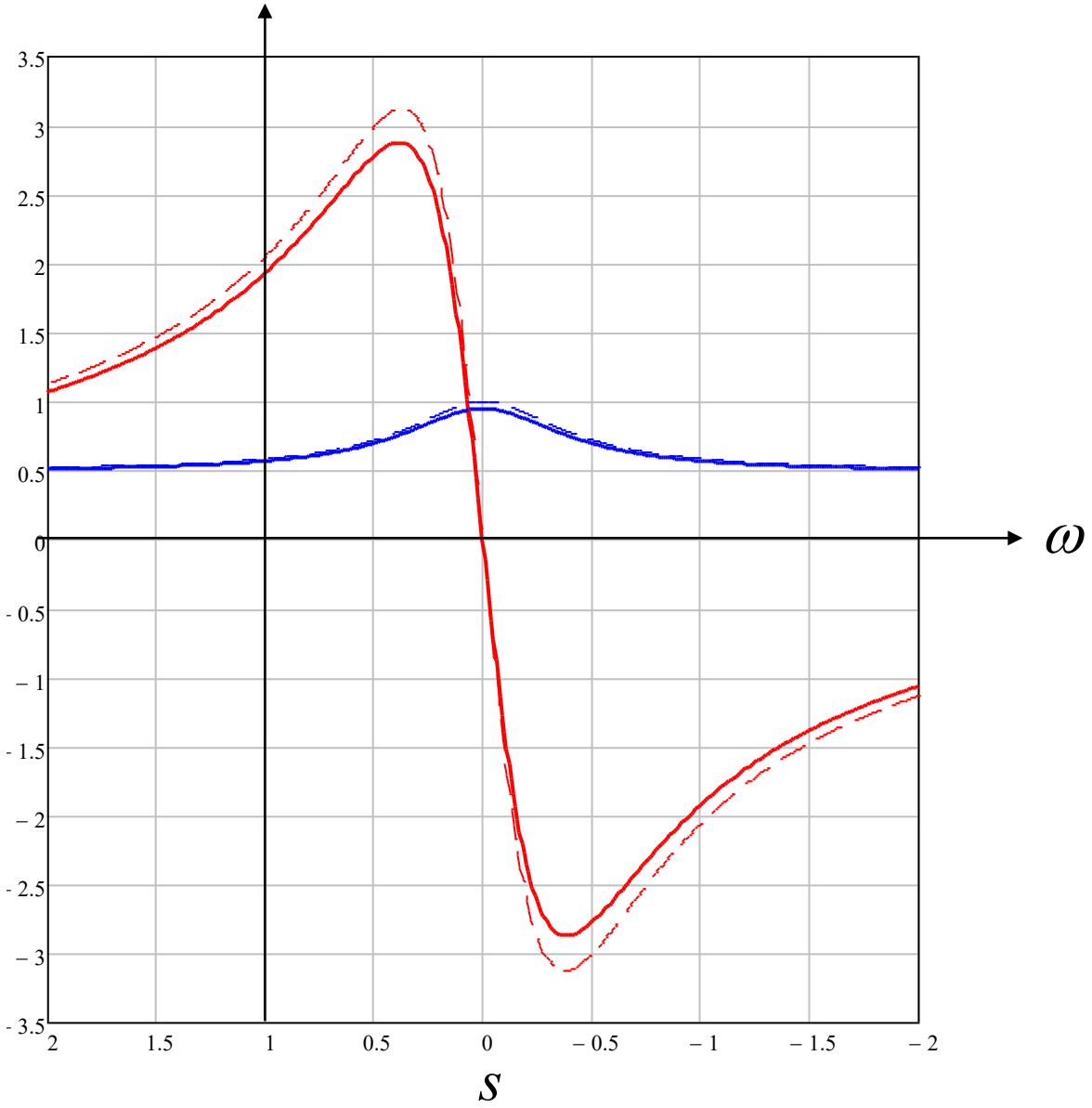
$R_s = 0$



$M_e(s)$ ——

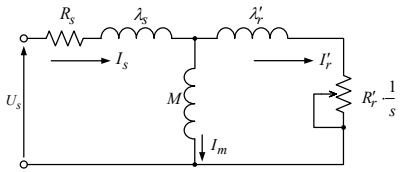
$|E(s)|$ ——





Statičke karakteristike struja, pri $E \neq \text{const.}$, $U_s = U_{sn} = \text{const.}$

$R_s = 0$



$|I_s(s)|$

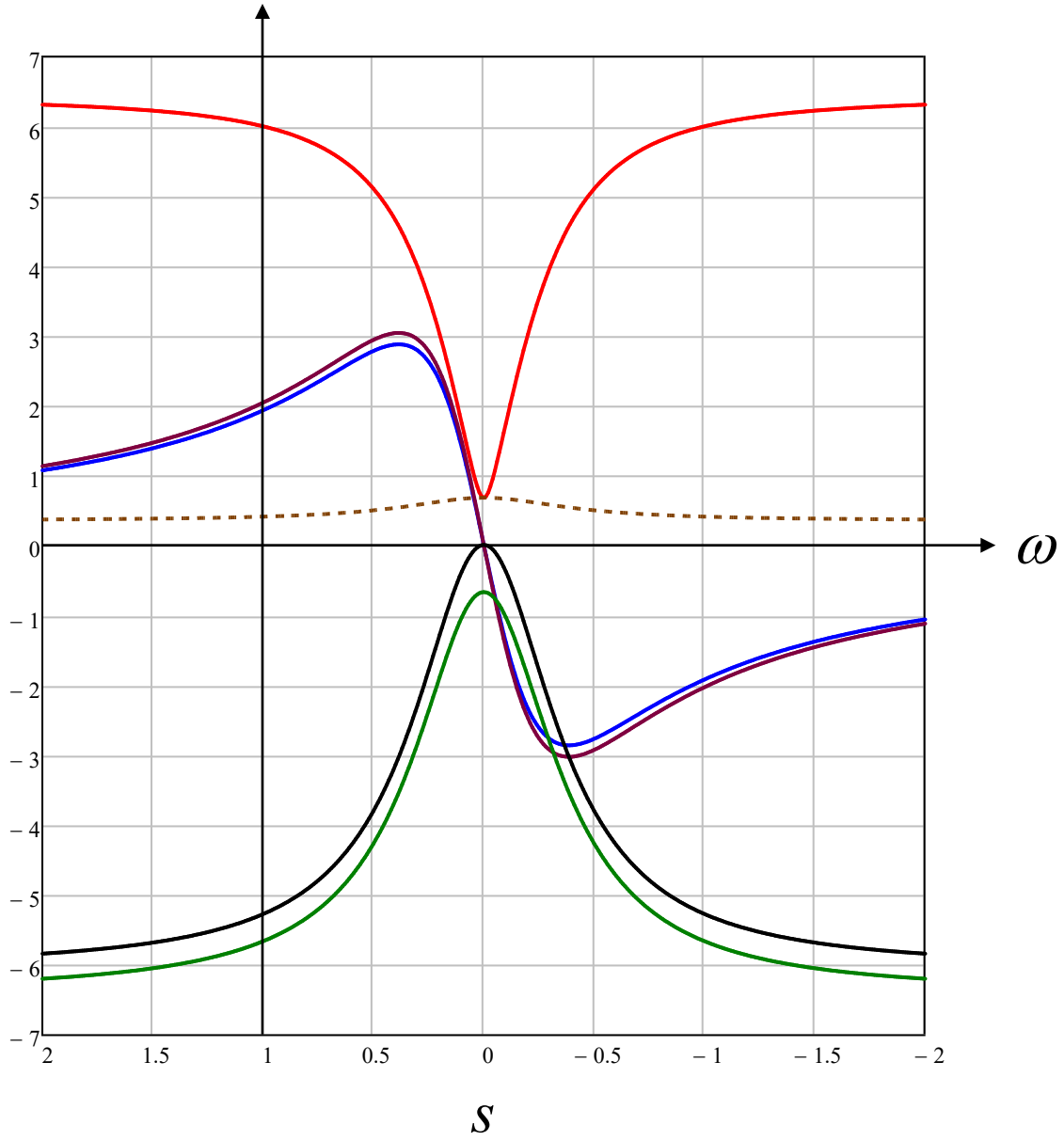
$\mathrm{Re}(I_s(s))$

$\mathrm{Re}(I_r(s))$

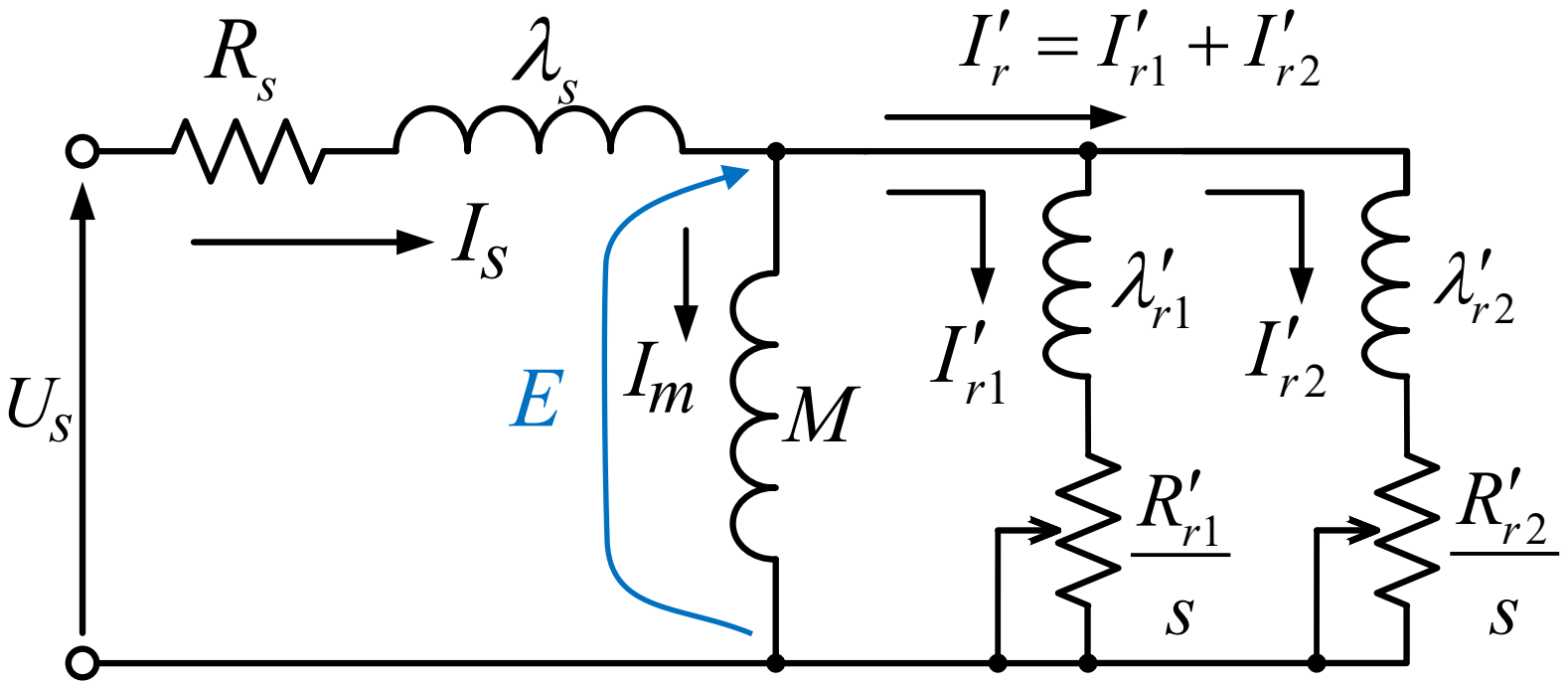
$\mathrm{Im}(I_s(s))$

$\mathrm{Im}(I_r(s))$

$|I_m(s)|$



Ekvivalentna šema (po fazi) kaveznog asinhronog motora sa dvostrukim rotorskim kavezom



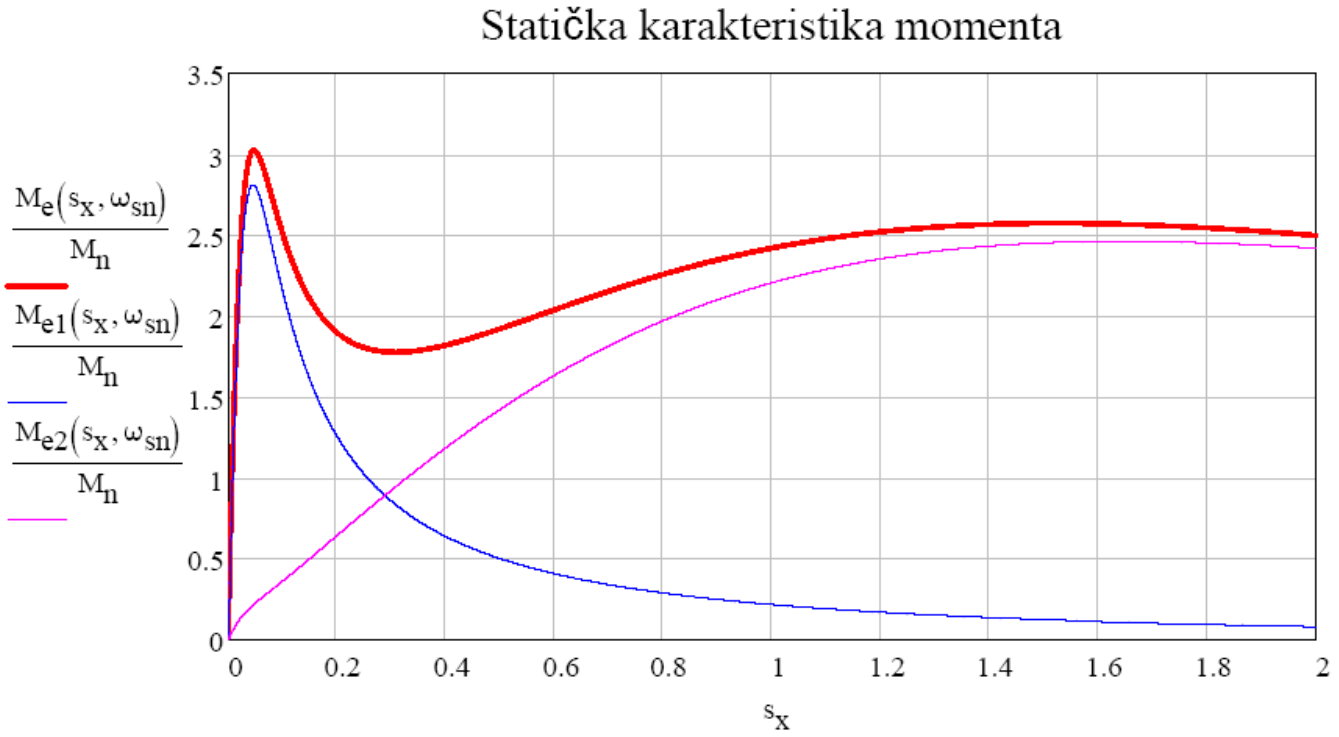
Zanemareni su gubici u gvožđu.

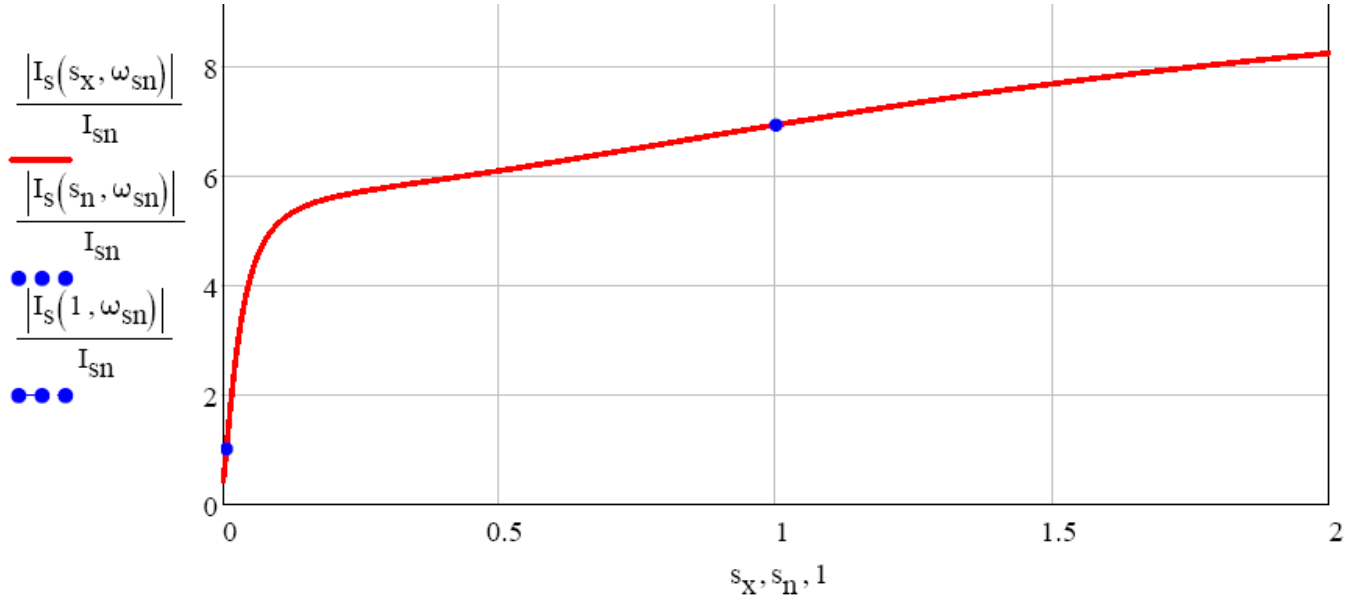
$$s = \omega_r / \omega_s = \left(\omega_s - \omega\right) / \omega_s$$

$$R'_{r1} \ll R'_{r2}$$

ABB
M3BP 315SMD 4
IE3

160 kW,
400 V,
50 Hz,
1489 o/min,
161 A,
1065 kg



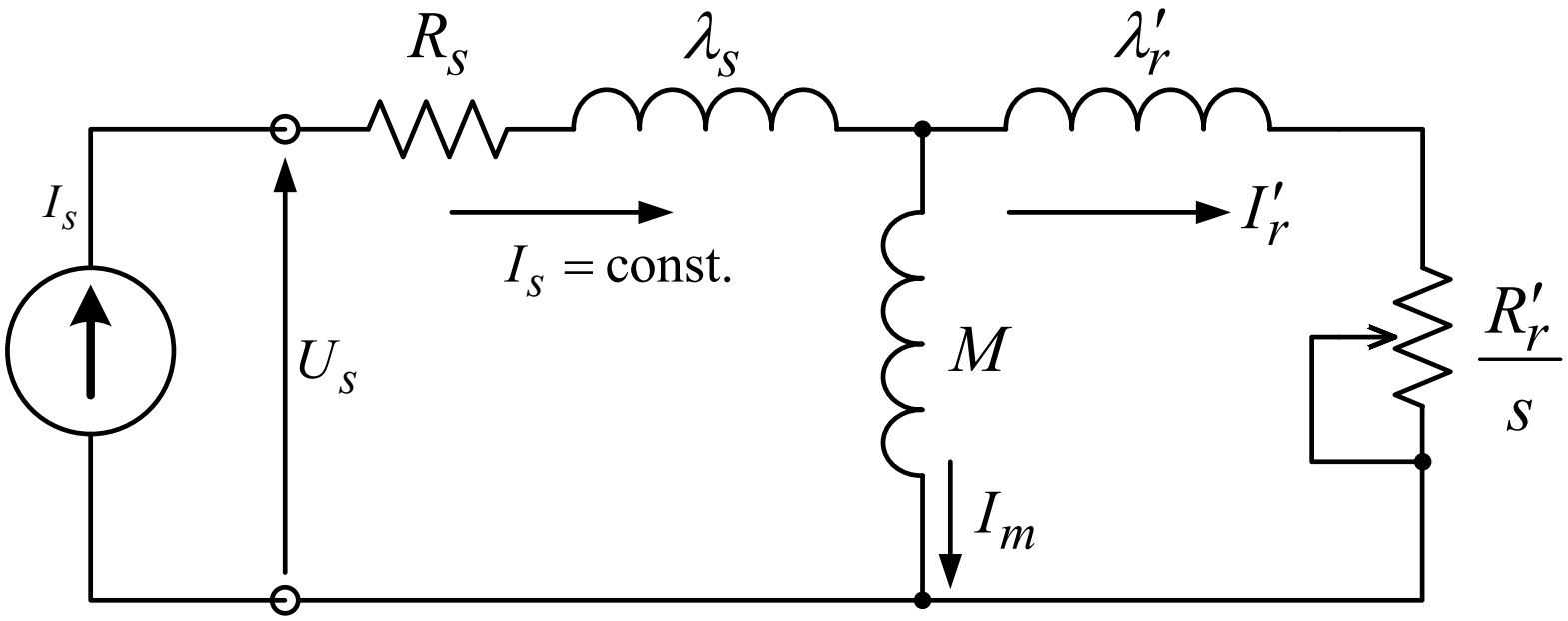


STRUJNO NAPAJANJE ASINHRONOG MOTORA

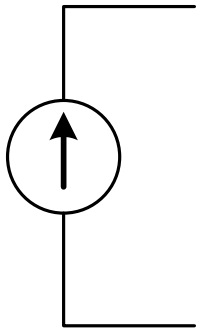
$$I_s = \text{const.}$$

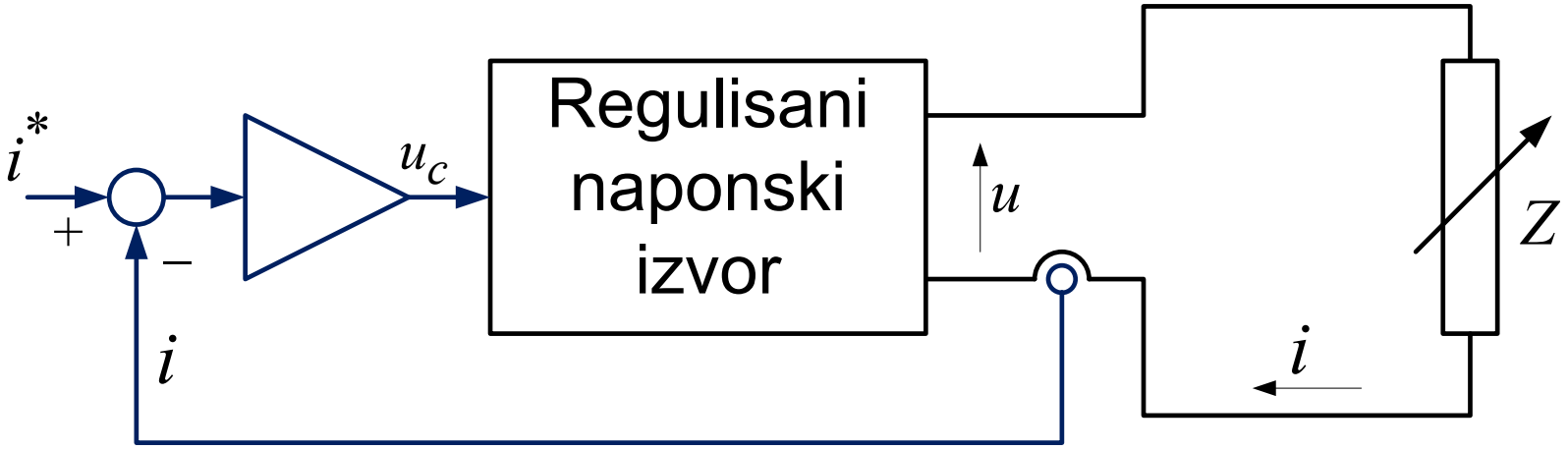
Ovakav način napajanja pruža nove mogućnosti kod napajanja iz invertora.

U analizi zanemarujemo gubitke u gvožđu. $P_{Fe} = 0$



Praktična realizacija strujnog generatora





Statička karakteristika momenta se izvodi iz:

$$\vec{I}_s = \vec{I}_m + \vec{I}'_r \qquad \vec{I}_m \cdot Z_m = \vec{I}'_r \cdot Z_r$$

$$\vec{I}'_r = \frac{Z_m}{Z'_r + Z_m} \cdot \vec{I}_s = \frac{j \cdot \omega_s \cdot M}{R'_r / s + j \cdot \omega_s \cdot \left(M + \lambda'_r \right)} \cdot \vec{I}_s$$

$$\left| \vec{I}'_r \right|^2 = \frac{\left(\omega_s \cdot M \right)^2}{\left(R'_r / s \right)^2 + \omega_s^2 \cdot \left(M + \lambda'_r \right)^2} \cdot \left| \vec{I}_s \right|^2 = \frac{\left(\omega_r \cdot M \right)^2}{\left(R'_r \right)^2 + \omega_r^2 \cdot \left(M + \lambda'_r \right)^2} \cdot \left| \vec{I}_s \right|^2$$

$$M_e = 3 \cdot P \cdot \frac{R'_r}{s} \frac{\omega_s \cdot M^2}{\left(\frac{R'_r}{s} \right)^2 + \omega_s^2 \cdot \left(M + \lambda'_r \right)^2} \cdot \left| \vec{I}_s \right|^2 =$$

$$= 3 \cdot P \cdot \frac{\omega_r \cdot R'_r \cdot M^2}{\left(R'_r \right)^2 + \omega_r^2 \cdot \left(M + \lambda'_r \right)^2} \cdot \left| \vec{I}_s \right|^2 = f\left(\omega_r, I_s \right)$$

Funkcija $M_e(s)$ ima ekstremum koji se može naći iz: $\dfrac{dM_e(s)}{ds} = 0$

Vrednosti prevalnog momenta i klizanja pri strujnom napajanju su:

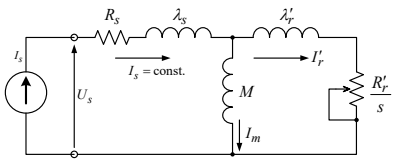
$$M_p = \pm \frac{3 \cdot P}{2} \cdot \left|\vec{I}_s\right|^2 \cdot \frac{M^2}{M + \lambda'_r} \qquad s_p = \pm \frac{R'_r}{\omega_s \cdot \left(M + \lambda'_r\right)}$$

Pomoću ovih prevalnih vrednosti može se izvesti odgovarajuća *KLOSS*-ova formula.

Mehanička karakteristika kod strujnog napajanja ima isti oblik kao i kod naponskog napajanja, ali se karakteristične vrednosti razlikuju.

$$\left.\begin{array}{l} s_{p\,nap.} > s_{p\,str.} \\ \\ M_{p\,nap.} > M_{p\,str.} \end{array}\right\} \quad \text{jer je} \quad M >> \lambda_s + \lambda'_r$$

Statička karakteristika momenta, pri strujnom napajanju $I_s = I_{sn}$



$\omega_s = \omega_{sn} = 1$

$M_{e\,str}(s)$

$M_{e\,nap}(s)$

naponska karakteristika $U_s = 1$

strujna karakteristika $I_s = 1$

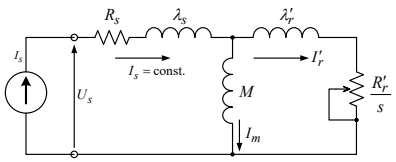
ZOOM

ω

s

3
2
1
0
– 1
– 2
– 3
– 4
2
1.5
1
0.5
0
– 0.5
– 1

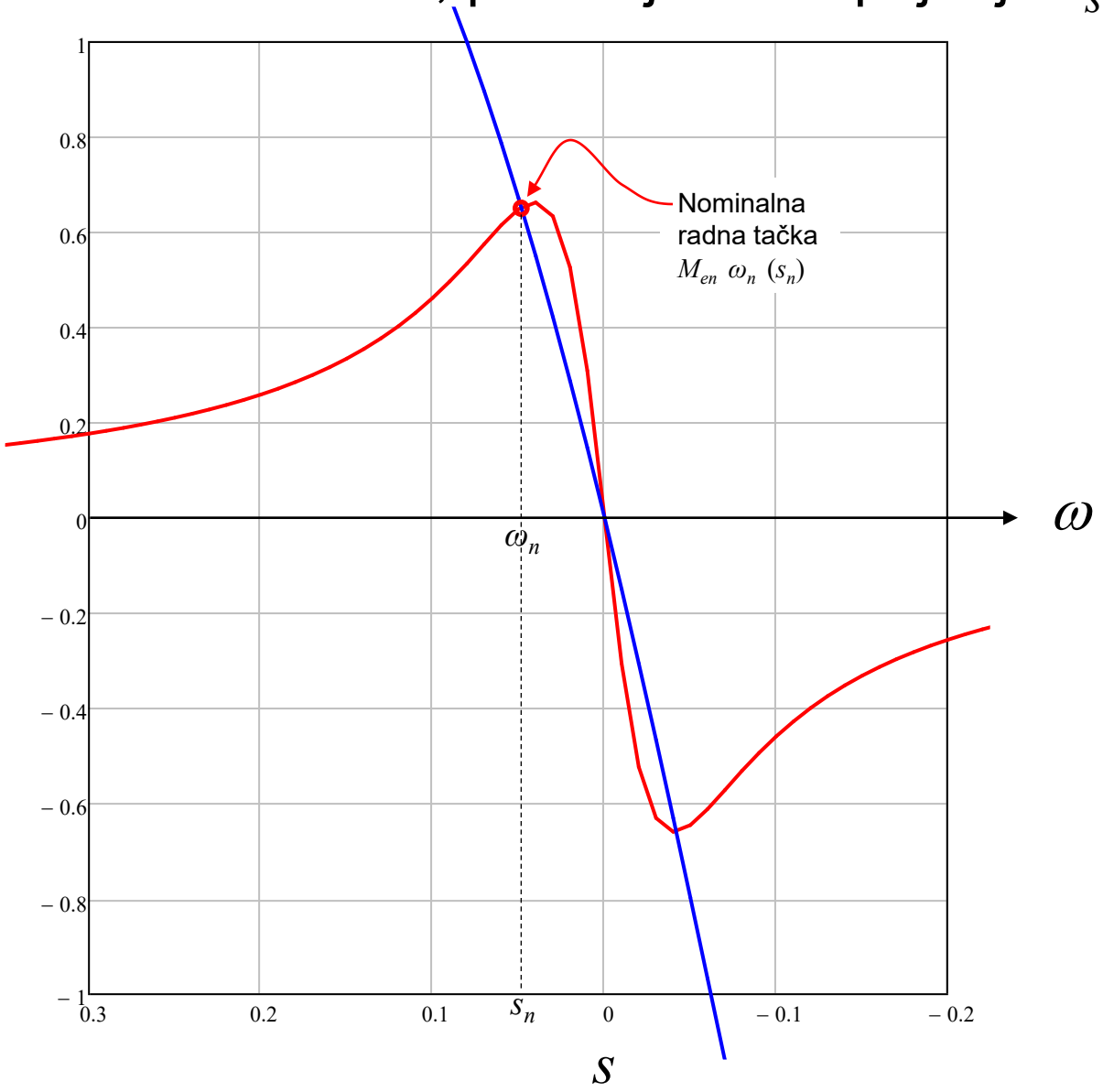
Statička karakteristika momenta, pri strujnom napajanju $I_s = I_{sn}$



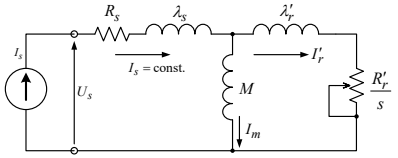
$$\omega_s = \omega_{sn} = 1$$

$M_{e\,str}(s)$

$M_{e\,nap}(s)$



Statičke karakteristike struja, pri strujnom napajanju $I_s = I_{sn}$



$|I_s(s)|$

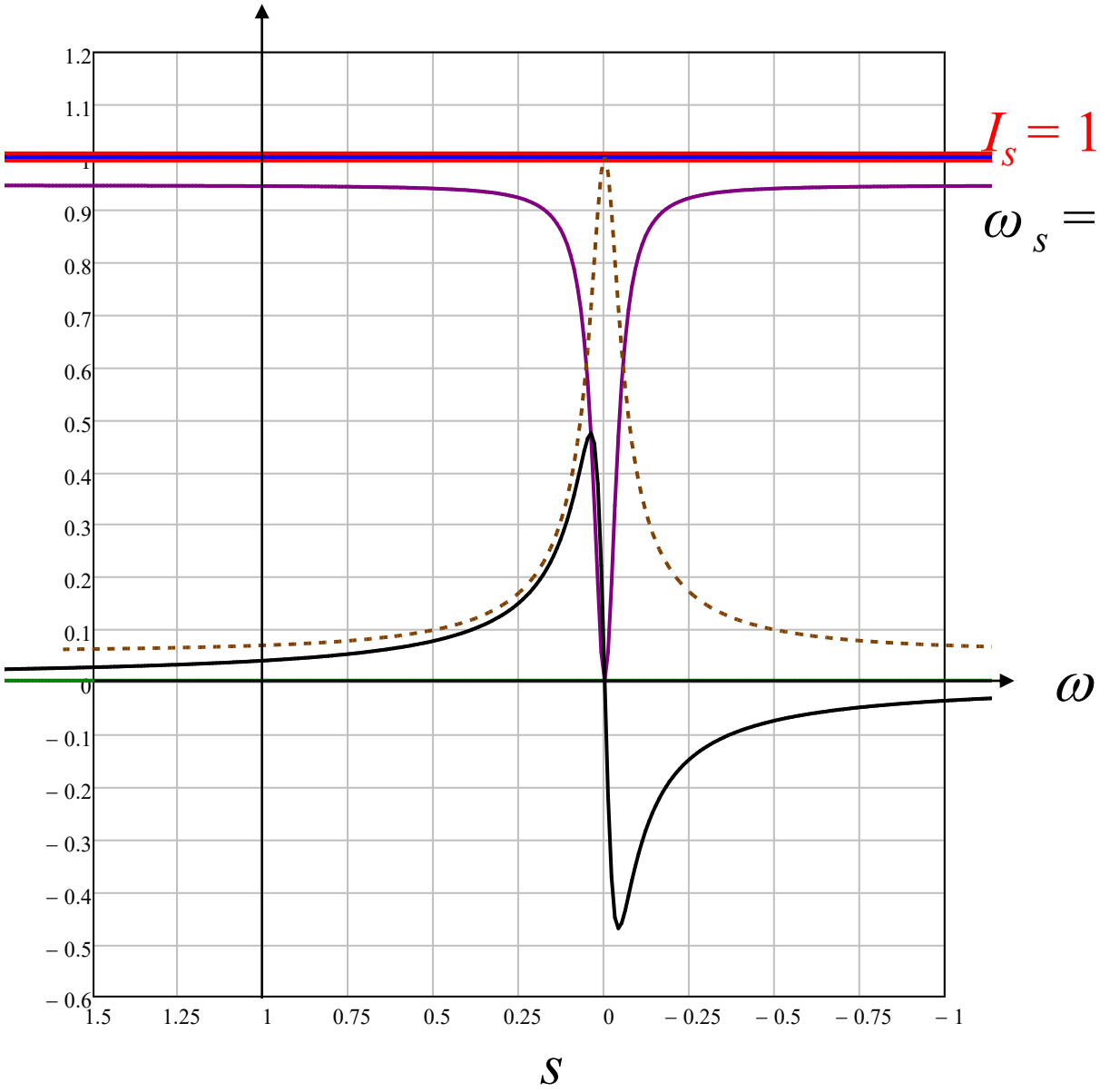
$\mathrm{Re}(I_s(s))$

$\mathrm{Re}(I_r(s))$

$\mathrm{Im}(I_s(s))$

$\mathrm{Im}(I_r(s))$

$|I_m(s)|$



$I_s = 1 + j \cdot 0$

$\omega_s = \omega_{sn} = 1$

STATIČKA KARAKTERISTIKA NAPONA

$$\vec{U}_s(s) = \vec{I}_s \cdot Z_{ekv}(s)$$

$$Z_{ekv}(s) = Z_s + Z_m \parallel Z'_r(s) =$$

$$= R_s + j \cdot \omega_s \cdot \lambda_s + \frac{j \cdot \omega_s \cdot M \cdot \left[\left(R'_r / s \right) + j \cdot \omega_s \cdot \lambda'_r \right]}{\left(R'_r / s \right) + j \cdot \omega_s \cdot \left(M + \lambda'_r \right)}$$

Uz uvažavanje $\lambda'_r \ll M \quad \Rightarrow \quad M - \lambda'_r \approx M$ može se napisati:

$$Z_{ekv}(s) = R_s + \frac{s \cdot \omega_s^2 \cdot M^2 \cdot R'_r}{\left(R'_r \right)^2 + s^2 \cdot \left(\omega_s \cdot M \right)^2} + j \cdot \omega_s \cdot \left(\lambda_s + \frac{s^2 \cdot \omega_s^2 \cdot \lambda'_r \cdot M^2 + M \cdot \left(R'_r \right)^2}{\left(R'_r \right)^2 + s^2 \left(\omega_s \cdot M \right)^2} \right)$$

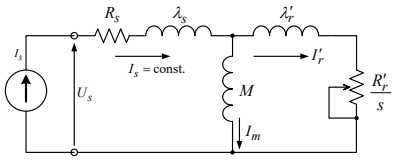
$$\lim_{s \to 0} Z_{ekv} = R_s + j \cdot \omega_s \cdot \left(\lambda_s + M \right)$$

$$\lim_{s \to 1} Z_{ekv} \approx R_s + R'_r + j \cdot \omega_s \cdot \left(\lambda_s + \lambda'_r \right)$$

jer je: $R'_r << \omega_s \cdot M$

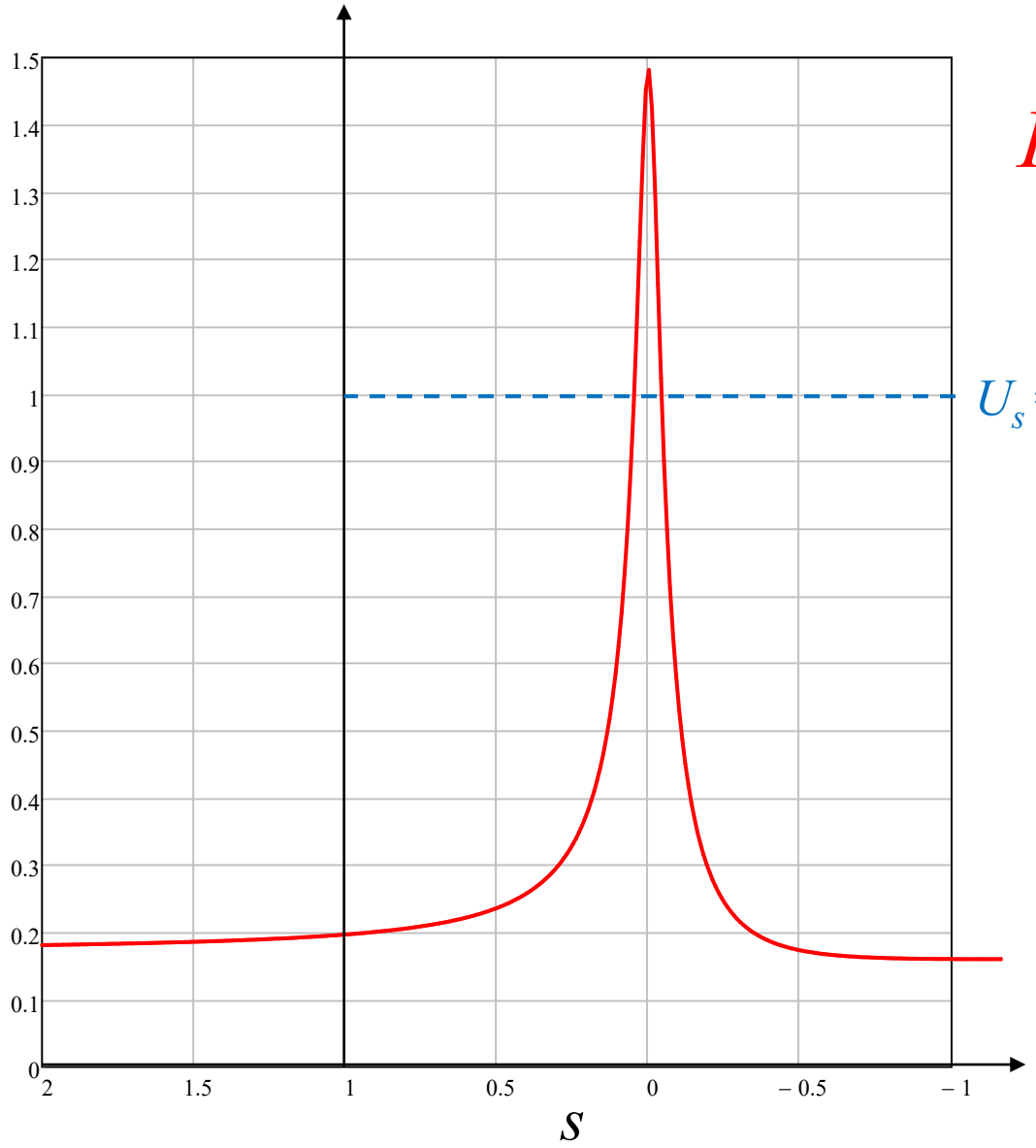
$$\left(R'_r \right)^2 << \left(\omega_s \cdot M \right)^2$$

Statička karakteristika napona statora kod strujno napajanog asinhronog motora pri nominalnoj struji



$$\omega_s = \omega_{sn} = 1$$

$$|U_s(s)|$$



$$I_s = I_{sn}$$

$$U_s = U_{sn} = 1$$

Da bi se održavala nominalna struja pri malim rotorskim učestanostima (malim vrednostima klizanja), potrebno je povećati napon preko nominalne vrednosti.